



**Report on the  
NCTPC  
2020–2030  
Collaborative  
Transmission  
Plan**

**December 14, 2020  
DRAFT REPORT**

# 2020 – 2030 NCTPC Transmission Plan

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# I. Executive Summary

The North Carolina Transmission Planning Collaborative (“NCTPC”) was established to:

- 1) provide the Participants (Duke Energy Carolinas (“DEC”), Duke Energy Progress (“DEP”), North Carolina Electric Membership Corporation (“NCEMC”), and ElectriCities of North Carolina (“ElectriCities”) and other stakeholders an opportunity to participate in the electric transmission planning process for the areas of North Carolina and South Carolina served by the Participants;
- 2) preserve the integrity of the current reliability and least-cost planning processes;
- 3) expand the transmission planning process to include analysis of increasing transmission access to supply resources inside and outside the Balancing Authority Areas (“BAAs”) of DEC and DEP; and
- 4) develop a single coordinated transmission plan for the Participants that includes Reliability and Local Economic Study Transmission Planning while appropriately balancing costs, benefits and risks associated with the use of transmission and generation resources.

The overall NCTPC Process is performed annually and includes the Reliability Planning and Local Economic Study Planning Processes, which are intended to be concurrent and iterative in nature. The NCTPC Process is designed such that there will be considerable feedback and iteration between the two processes as each effort’s solution alternatives affect the other’s solutions.

The 2019–2029 Collaborative Transmission Plan (the “2019 Collaborative Transmission Plan” or the “2019 Plan”) was published in January 2019.

This report documents the current 2020 – 2030 Collaborative Transmission Plan (“2020 Collaborative Transmission Plan” or the “2020 Plan”) for the Participants. The

initial sections of this report provide an overview of the NCTPC Process as well as the specifics of the 2020 reliability planning study scope and methodology. The NCTPC Process document and 2020 Study scope document are posted in their entirety on the NCTPC website at <http://www.nctpc.org/nctpc/>.

The scope of the 2020 reliability planning process was focused on the annual base reliability study. The base reliability study assessed the reliability of the transmission systems of both DEC and DEP in order to ensure reliability of service in accordance with North American Electric Reliability Corporation (“NERC”), SERC Reliability Corporation (“SERC”), and DEC and DEP requirements. The purpose of the base reliability study was to evaluate the transmission systems’ ability to meet load growth projected for 2020 through 2030 with the Participants’ planned Designated Network Resources (“DNRs”).

Based on the study’s input assumptions, the 2020 Study allowed for identification of any new system impacts not currently addressed by existing transmission plans, in which case solutions were developed. The 2020 Study also allowed for adjustments to existing plans where necessary.

The NCTPC reliability study results affirmed that the planned DEC and DEP transmission projects identified in the 2019 Plan continue to satisfactorily address the reliability concerns identified in the 2019 Study for the near-term (5 year) and the long-term (10 year) planning horizons. The 2020 Plan is detailed in Appendix B which identifies the new and updated projects planned with an estimated cost of greater than \$10 million.

The total estimated cost for the 17 reliability projects included in the 2020 Plan is \$804 million as documented in Appendix B. This compares to the original 2019 Plan estimate of \$591 million for 14 reliability projects. In-service dates and cost estimates for some projects that are planned or underway have been revised based on updated information. An update to the 2019 plan was provided in the 2020 mid-year update published in June 2020 with an updated cost estimate of \$632 million. See Appendix D for a detailed comparison of this year’s Plan to the updated 2019 Plan.

The list of major projects will continue to be modified on an ongoing basis as new improvements are identified through the NCTPC Process and projects are placed in-service or eliminated from the list. Appendix C provides a more detailed description of each project in the 2020 Plan.

The 2020 Plan, relative to the 2019 Plan, includes 1 new DEC project:

- South Point Switching Station

The 2020 Plan, relative to the 2019 Plan, includes 5 new DEP projects:

- Wateree 115 kV Plant, Upgrade 115/100 kV Transformers.
- Carthage 230/115 kV Substation, Construct substation and loop-in Cape Fear–West End 230 kV line and West End–Southern Pines 115 kV Feeder.
- Falls 230 kV Substation, Add 300 MVAR Static Var Compensator.
- Castle Hayne–Folkstone 115 kV line, rebuild 556 MCM and 6-(2/0) copper sections to 1272 ACSR.
- Holly Ridge North 115 kV SS, construct station, loop in Castle Hayne–Folkstone 115 kV and Folkstone–Jacksonville City 115 kV, and build 0.5 mile 115 kV feeder to Jones–Onslow EMC Folkstone POD

There are revised in-service dates, estimated cost changes, and/or scope changes for the following DEC and DEP projects:

- Durham–RTP 230 kV Line project had an increase in estimated cost.
- Jacksonville–Grants Creek 230 kV Line and Grants Creek 230/115 kV Substation project was placed in-service.
- Newport–Harlowe 230 kV Line, Newport SS and Harlowe 230/115 kV Substation project was placed in-service.

- Sutton–Castle Hayne 115 kV North line project had a decrease estimated lead time.
- Asheboro–Asheboro East 115 kV North Line project had a small increase in estimated cost and its in-service date was pushed out.
- Rural Hall 100 kV SVC project was placed in-service.
- Orchard 230/100 kV Tie Station project was placed in-service.
- Windmere 100 kV Line (Dan River–Sadler) project had a decrease in estimated cost and its in-service date was pushed out.
- Wilkes 230/100 kV Tie Station project had an increase in estimated cost and its in-service date was pushed out.
- Craggy–Enka 230 kV Line project in-service date was pushed out.
- Cokesbury 100 kV Line (Coronaca–Hodges) project had a decrease in estimated cost and its in-service date was pushed out.

The following DEP project has been removed:

- Brunswick #1–Jacksonville 230 kV Line, Loop into Folkstone 230 kV Substation

For a variety of reasons (such as load growth, generation retirements, or power purchase agreements expiring), LSEs may wish to evaluate other resource supply options to meet future load demand as part of the Local Economic Study Process. These resource supply options can be either in the form of transactions or some hypothetical generators which are added to meet the resource adequacy requirements for this study. For the 2020 Study, the NCTPC evaluated a local economic impact of rapid high load growth (5–6% growth) occurring in the Union and Cabarrus County areas of North Carolina for the 2025 and 2030 summer models.

Each year, the Oversight Steering Committee (“OSC”) will determine if there are any public policies driving the need for local transmission upgrades. Through this process

the OSC will seek input from Transmission Advisory Group (“TAG”) participants to identify any public policy impacts to be evaluated as part of the Local Planning Process. The OSC may itself identify public policies to be evaluated. For the 2020 Study, the Southeast Wind Coalition identified a public policy involving NC offshore wind development. As a result of this request, the NCTPC decided to evaluate the local public policy impacts of an NC offshore wind development as follows:

- the potential for 2,400 MW of wind generation injecting into Dominion’s Landstown 230 kV area to be wheeled into the DEC/DEP areas (60%/40% ratio); and
- separately, determine 3 least-cost injection points along the NC coast and determine the transmission cost breakpoints for varying amounts of generation injection at those sites up to 5,000 MW, also split to DEC 60% and DEP 40%.

The analysis of this public policy impact was not completed in time for inclusion in this report. The NC offshore wind study results will be provided in a separate report once the full analysis is completed in early 2021.

In this 2020 NCTPC Process, the Participants validated and continued to build on the information learned from previous years’ efforts. Each year the Participants will look for ways to improve and enhance the planning process. The study process confirmed again this year that the joint planning approach produces benefits for all Participants that would not have been realized without a collaborative effort.

## **II. North Carolina Transmission Planning Collaborative Process**

### ***II.A. Overview of the Process***

The NCTPC Process was established by the Participants to:

- 1) provide the Participants (DEC, DEP, NCEMC, and Electricities) and other stakeholders an opportunity to participate in the electric transmission planning process for the areas of North Carolina and South Carolina served by the Participants;
- 2) preserve the integrity of the current reliability and least-cost planning processes;
- 3) expand the transmission planning process to include analysis of increasing transmission access to supply resources inside and outside the Balancing Authority Areas of DEC and DEP; and
- 4) develop a single coordinated transmission plan for the Participants that includes reliability and economic considerations while appropriately balancing costs, benefits, and risks associated with the use of transmission and generation resources.

The NCTPC Process is a coordinated Local Transmission Planning process conducted on an annual basis. The entire, iterative process ultimately results in a single Local Transmission Plan that appropriately balances the costs, benefits, and risks associated with the use of transmission, generation, and demand-side resources. The Local Transmission Plan will identify local transmission projects (Local Projects). A Local Project is defined as a transmission facility that is (1) located solely within the combined DEC–DEP transmission system footprint and (2) not selected in the regional transmission plan for purposes of regional cost allocation.



The Local Planning Process addresses transmission upgrades needed to maintain reliability and to integrate new generation resources and/or loads. The overall Local Planning Process includes several components:

- Reliability Planning Process
- Resource Supply Options Process
- Local Economic Study Process
- Local Public Policy Process

The Reliability Planning Process (base reliability study) evaluates each Transmission System's ability to meet projected load with a defined set of resources as well as the needs of firm point-to-point customers, whose needs are reflected in their transmission contracts and reservations. The Resource Supply Options Process is conducted to evaluate transmission system impacts for other potential resource supply options to meet future load requirements.

The overall Local Planning Process is designed such that there will be considerable feedback and iteration between the Reliability Planning Process and Resource Supply Options Process. This is necessary as the alternative solutions from one process affect the alternative solutions in the other process.

The Local Economic Study Process allows the TAG participants to propose economic upgrades to be studied as part of the Local Planning Process. This process evaluates the means to increase transmission access to potential supply resources inside and outside the Balancing Authority Areas of the DEC and DEP. This economic analysis provides the opportunity to study the transmission upgrades that would be required to reliably integrate new resources.

The Local Public Policy Process identifies if there are any public policies that are driving the need for local projects. Either the OSC or the TAG could identify those public policies that may drive the need for local transmission.

The OSC manages the NCTPC Process. The Planning Working Group (“PWG”) implements the development of the NCTPC Process and coordinates the study development. The TAG provides advice and makes recommendations regarding the development of the NCTPC Process and the study results.

The final results of the Local Planning Process include summaries of the estimated costs and schedules to provide any transmission upgrades and/or additions needed to maintain a sufficient level of reliability necessary to serve customers. Throughout the Local Planning Process, TAG participants (including TAG participants representing transmission solutions, generation solutions, and solutions utilizing demand resources) may participate.

The purpose of the NCTPC Process is more fully described in the current Participation Agreement which is posted at <http://www.nctpc.org/nctpc/>.

## ***II.B. Reliability Planning Process and Resource Supply Options Process***

The Reliability Planning Process is the Transmission Planning Process that has traditionally been used by the transmission owners to provide safe and reliable transmission service at the lowest reasonable cost. Through the NCTPC, this Transmission Planning Process was expanded to include the active participation of the Participants and input from other stakeholders through the TAG.

The Reliability Planning Process is designed to follow the steps outlined below. The OSC approves the scope of the reliability study, oversees the study analysis being performed by the PWG, evaluates the study results, and approves the final reliability study results. The Reliability Planning Process begins with the incumbent transmission owners’ most recent reliability planning studies and planned transmission upgrade projects.

In addition, the PWG solicits input from the Participants for different scenarios on where to include alternative supply resources to meet their load demand forecasts in the study. This is known as the Resource Supply Options Process. This step provides the opportunity for the Participants to propose the evaluation of other resource supply options to meet future load demand due to load growth, generation retirements, or the expiration of purchase power agreements. The PWG analyzes the proposed interchange transactions and/or the location of generators to determine if those transactions or generators create any reliability criteria violations. Based on this analysis, the PWG provides feedback to the Participants on the viability of the proposed interchange transactions or generator locations for meeting future load requirements. Note that new or modified interchange or generation must go through official FERC, NC, or SC Generator Interconnection or Transmission Service processes, which may find different results than the NCTPC study process. The PWG coordinates the development of the reliability study and the resource supply option study based upon the OSC approved scope and prepares a report with the recommended transmission reliability solutions.

The overall Local Planning Process is designed such that there will be considerable feedback and iteration between the Reliability Planning Process and the Resource Supply Options Process. This is necessary as the alternative solutions from one process may affect the alternative solutions in the other process.

The results of the Reliability Planning Process include summaries of the estimated costs and schedules to provide transmission upgrades and/or additions: (i) needed to maintain a sufficient level of reliability necessary to serve the native load of all Participants and (ii) needed to reliably support the resource supply options studied. The reliability study results are reviewed with the TAG, and the TAG participants are given an opportunity to provide comments on the results. All TAG feedback is reviewed by the OSC for consideration for incorporation into the final Collaborative Transmission Plan.

For the 2020 Study, the NCTPC evaluated no resource supply scenarios as no resource supply scenario requests were received by the Participants by the deadline of February 5, 2020. Resource supply scenarios will be solicited again for the 2021 Study and included if appropriate.

## ***II.C. Local Economic Study Process***

The Local Economic Study Process allows the TAG participants to propose hypothetical economic transfers to be studied as part of the Local Planning Process. The Local Economic Study Process provides the means to evaluate the impact of potential supply resources inside and outside the BAAs of the Transmission Providers. This local economic analysis provides the opportunity to study what transmission upgrades would be required to reliably integrate new resources.

The Local Economic Study Process begins with the TAG members proposing scenarios and interfaces to be studied. The proposed scenarios and interfaces are compiled by the PWG and then evaluated by the OSC to determine which ones will be included for analysis in the current planning cycle.

The OSC approves the scope of the local economic study scenarios (including any changes in the assumptions and study from those used in the reliability analysis), oversees the study analysis being coordinated by the PWG, evaluates the study results, and approves the final local economic study results.

The PWG coordinates the development of the local economic studies based upon the OSC approved scope and prepares a report which identifies recommended transmission solutions that could increase transmission access.

The results of the Local Economic Study Process include the estimated costs and schedules to provide the increased transmission capabilities.

The local economic study results are reviewed with the TAG, and the TAG participants are given an opportunity to provide comments on the results. All TAG feedback is reviewed by the OSC for consideration for incorporation into the final Local Transmission Plan.

While the overall NCTPC Process includes both a Reliability Planning Process and the Local Economic Study Process, some planning cycles may only focus on the Reliability Planning Process if stakeholders do not request any economic study scenarios for a particular planning cycle.

For the 2020 Study, the NCTPC evaluated a local economic impact of rapid high load growth (5–6% growth) occurring in the Union and Cabarrus County areas of North Carolina for the 2025 and 2030 summer models.

#### ***II.D. Local Public Policy Process***

Each year, the OSC will determine if there are any public policies driving the need for local transmission upgrades. Through this process the OSC will seek input from TAG participants to identify any public policy impacts to be evaluated as part of the Local Planning Process. The OSC may itself identify public policies to be evaluated. The OSC will use the criteria below to determine if there are any public policies driving the need for local transmission as follows:

- The public policy must be reflected in state, federal, or local law or regulation (including order of a state, federal, or local agency).
- There must be existence of facts showing that the identified need cannot be met absent the construction of additional transmission facilities.

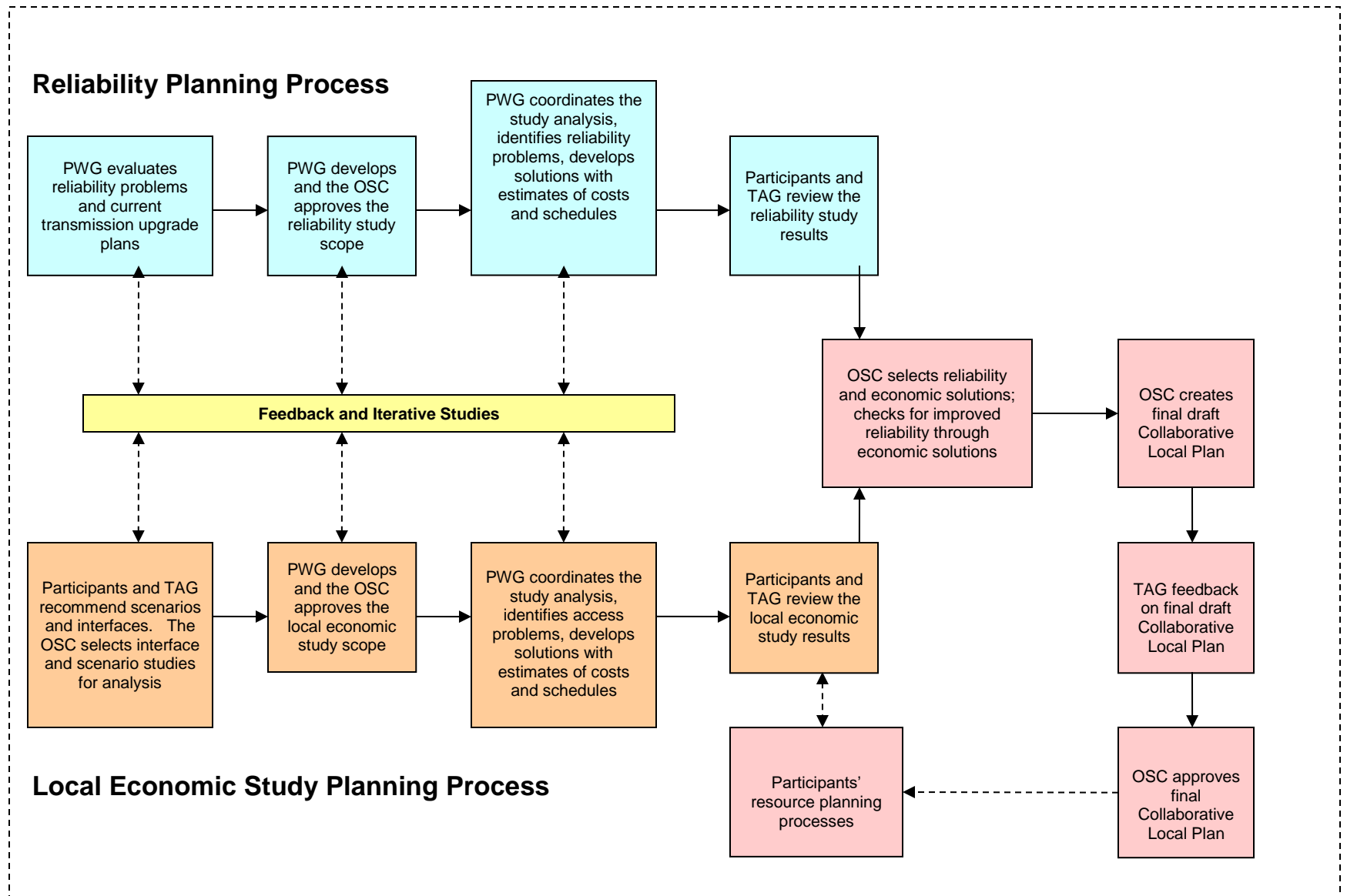
For the 2020 Study, the NCTPC evaluated local public policy impacts of an offshore wind development as follows:

- the potential for 2,400 MW of wind generation injecting into Dominion’s Landstown 230 kV area to be wheeled into the DEC/DEP areas (60/40 ratio); and

- separately, determine 3 least-cost injection points along the NC coast and determine the transmission cost breakpoints for varying amounts of generation injection at those sites up to 5,000 MW, also split to DEC 60% and DEP 40%.

The analysis of this public policy impact was not completed in time for inclusion in this report. The NC offshore wind study results will be provided in a separate report once the full analysis is completed in early 2021.

## 2020 NCTPC Process Flow Chart



## ***II.E. Local Transmission Plan***

Once the reliability and local economic studies are completed, including any evaluations due to public policies, the OSC evaluates the results and the PWG recommendations to determine if any proposed economic projects and/or resource supply option projects will be incorporated into the Local Transmission Plan. If so, the initial plan developed based on the results of the reliability studies is modified accordingly. This process results in a single Local Transmission Plan being developed that appropriately balances the costs, benefits and risks associated with the use of transmission and generation resources. This plan is reviewed with the TAG, and the TAG participants are given an opportunity to provide comments. All TAG feedback is reviewed by the OSC for consideration for incorporation into the final Local Transmission Plan.

The annual Local Transmission Plan information is available to Participants for identification of any alternative least cost resources for potential inclusion in their respective Integrated Resource Plans. Other stakeholders can similarly use this information for their resource planning purposes.



### III. 2020 Reliability Planning Study Scope and Methodology

The scope of the 2020 Reliability Planning Process was focused on the annual base reliability study. The base reliability study assessed the transmission systems of both DEC and DEP in order to ensure reliability of service in accordance with North American Electric Reliability Corporation (“NERC”), SERC Reliability Corporation (“SERC”), and DEC and DEP requirements. The purpose of the base reliability study was to evaluate the transmission systems’ ability to meet load growth projected for 2025 summer through 2030 summer with the Participants’ planned Designated Network Resources (“DNRs”). The 2020 Study allowed for identification of any new system impacts not currently addressed by existing transmission plans in which case solutions were developed. The 2020 Study also allowed for adjustments to existing plans where necessary.

#### III.A. Assumptions

##### 1. Study Year and Planning Horizon

The 2020 Plan addressed a ten-year planning horizon through 2020. The study years chosen for the 2020 Study are listed in Table 1.

**Table 1**  
**Study Years**

<b>Study Year / Season</b>	<b>Analysis</b>
2025 Summer	Near-term base reliability
2025/2026 Winter	Near-term base reliability
2030 Summer	Long-term base reliability

To identify projects required in years other than the base study years of 2025, 2025/2026 and 2030, line loading results for those base study years

were extrapolated into future years assuming the line loading growth rates in Table 2. This allowed assessment of transmission needs throughout the planning horizon. The line loading growth rates are based on each BAAs individual load growth projection at the time the study process was initiated.

**Table 2**  
**Line Loading Growth Rates**

Company	Line Loading Growth Rate
DEC <sup>1</sup>	1.2% per year (summer) 1.2% per year (winter)
DEP	1.0% per year (summer) 0.9% per year (winter)

## 2. Network Modeling

The network models developed for the 2020 Study included new transmission facilities and upgrades for the 2025, 2025/2026, and 2030 models, as appropriate, from the current transmission plans of DEC and DEP and from the 2019 Plan. Table 3 lists the planned major transmission facility projects (with an estimated cost of \$10 million or more each) included in the 2025, 2025/2026, and 2030 models. Table 4 lists the generation facility changes included in the 2025, 2025/2026, and 2030 models.

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<sup>1</sup> For the purpose of planning a transmission system with appropriate robustness, DEC line loading growth rates shown in Table 2 exceed the growth rates provided in DEC’s IRP.

**Table 3  
Major Transmission Facility Projects Included in Models**

<b>Company</b>	<b>Transmission Facility</b>	<b>2025</b>	<b>2030</b>
DEC	Orchard Tie 230/100 kV Tie Station, Construct	Yes	Yes
DEC	Wilkes 230/100 kV Tie Station, Construct	Yes	Yes
DEC	Cokesbury 100 kV Line (Coronaca–Hodges), Upgrade	No	Yes
DEC	South Point Switching Station, Construct	No	Yes
DEP	Jacksonville–Grants Creek 230 kV Line, Grants Creek 230/115 kV Substation	Yes	Yes
DEP	Newport–Harlowe 230 kV Line, Newport Switching Station, Harlowe 230/115 kV Substation	Yes	Yes
DEP	Sutton–Castle Hayne 115 kV North line rebuild	Yes	Yes
DEP	Asheville Plant, Replace 2-300 MVA 230/115 kV banks with 2-400 MVA banks, reconductor 115 kV ties to switchyard, upgrade breakers, and add 230 kV capacitor bank	Yes	Yes
DEP	Cane River 230 kV Substation, Construct 150 MVAR SVC	Yes	Yes
DEP	Asheboro–Asheboro East 115 kV North Line, Reconductor	Yes	Yes
DEP	Craggy–Enka 230 kV Line, Construct	No	Yes

**Table 4**  
**Major Generation<sup>2</sup> Facility Changes in Models**

<b>Company</b>	<b>Generation Facility</b>	<b>2025</b>	<b>2030</b>
DEC	Added Lincoln County CT (525 MW)	Yes	Yes
DEC	Added Reidsville Energy Center (477 MW)	Yes	Yes
DEC	Retired Allen 1-3 (617 MW)	Yes	Yes
DEC	Retired Allen 4-5 (564 MW)	No	Yes
DEC	Added Apex PV (30 MW)	Yes	Yes
DEC	Added Broad River PV (50 MW)	Yes	Yes
DEC	Added Cool Springs PV (80 MW)	Yes	Yes
DEC	Added Gaston PV (25 MW)	Yes	Yes
DEC	Added High Shoals PV (16 MW)	Yes	Yes
DEC	Added Lancaster PV (10 MW)	Yes	Yes
DEC	Added Lick Creek PV (50 MW)	Yes	Yes
DEC	Added Maiden Creek PV (69.3 MW)	Yes	Yes
DEC	Added Oakboro PV (40 MW)	Yes	Yes
DEC	Added Partin PV (50 MW)	Yes	Yes
DEC	Added Pelham PV (32 MW)	Yes	Yes
DEC	Added Pinson PV (20 MW)	Yes	Yes
DEC	Added Ruff PV (22 MW)	Yes	Yes
DEC	Added Speedway PV (22.6 MW)	Yes	Yes
DEC	Added Stanly PV (50 MW)	Yes	Yes
DEC	Added Stony Knoll PV (22.6 MW)	Yes	Yes
DEC	Added Sugar PV (60 MW)	Yes	Yes
DEC	Added Thinking Tree (35 MW)	Yes	Yes
DEC	Added Two Hearted PV (22 MW)	Yes	Yes

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<sup>2</sup> Major Generation Threshold is considered to be 10 MW or greater and connected to the transmission system

<b>Company</b>	<b>Generation Facility</b>	<b>2025</b>	<b>2030</b>
DEC	Added West River PV (40 MW)	Yes	Yes
DEC	Added Westminster PV (75 MW)	Yes	Yes
DEP	Retired Asheville 1-2 (380 MW)	Yes	Yes
DEP	Retired Darlington Co 1, 2, 3, 4, 6, 7, 8, 10 (514 MW)	Yes	Yes
DEP	Retired Blewett CTs 1-4 and Weatherspoon CTs 1-4 (232 MW)	Yes	Yes
DEP	Retired Roxboro Units 1-2 (1053 MW)	No	Yes
DEP	Added Asheville CC (2 x 280 MW)	Yes	Yes
DEP	Added Crooked Run Solar (70.1 MW)	Yes	Yes
DEP	Added Bay Tree Solar (70.1 MW)	Yes	Yes

### **3. Interchange and Generation Dispatch**

Each Participant provided a resource dispatch order for each of its DNRs for the DEC and DEP BAAs. Generation was dispatched for each Participant to meet that Participant's load in accordance with the designated dispatch order.

DEC models distribution-connected generation as being netted against the load at the transmission bus. Transmission-connected generation is modeled if it is either in-service or has an executed generator interconnection agreement at the time the models are built. Because only transmission-connected generation is modeled explicitly, the following assumptions do not apply to distribution-connected generation. Solar generation is available for dispatch up to the generator interconnection agreement value but is only dispatched at 80% of that value in summer models. Facilities with storage may be dispatched up to 100% of the generator interconnection agreement value depending on the amount of storage associated with the facility. This level of dispatch is jurisdiction-specific and is supported by operating data that can be reflective of various factors such as geography and plant design. Solar generation is not

dispatched in winter models. These dispatch assumptions reflect the expected solar generation output coincident with the DEC peak load. DEC models 1098 MW of transmission-connected solar generation available for dispatch, dispatched consistent with the aforementioned dispatch assumptions.

DEP models solar generation in its power flow cases that is either in-service or has an executed generator interconnection agreement at the time the models are built. This includes transmission-connected as well as distribution-connected solar generation. The current 2025 summer power flow case has approximately 994 MW of transmission-connected and 1789 MW of distribution-connected solar generation for a total of 2783 MW. In its summer peak cases, DEP scales the solar generation down to 50% of its maximum capacity to approximate the amount of solar generation that will be on-line coincident with the DEP peak load. This level of dispatch is jurisdiction-specific and is supported by operating data that can be reflective of various factors such as geography and plant design. For winter peak studies, DEP assumes that no solar generation will be available at the time of the winter peak. DEP models all transmission upgrades that are determined necessary by the respective generation interconnection studies.

### ***III.B. Study Criteria***

The results of the base reliability study, the resource supply option study, and the local economic study were evaluated using established planning criteria. The planning criteria used to evaluate the results include:

- 1) NERC Reliability Standards;
- 2) SERC requirements; and
- 3) Individual company criteria.

### ***III.C. Case Development***

The base case for the base reliability study was developed using the most current 2019 series NERC Multiregional Modeling Working Group (“MMWG”) model for the systems external to DEC and DEP. The MMWG model of the external systems, in accordance with NERC MMWG criteria,

included modeling known long-term firm transmission reservations. Detailed internal models of the DEC and DEP East/West systems were merged into the base case, including DEC and DEP transmission additions planned to be in service by the period under study. In the base cases, all confirmed long-term firm transmission reservations with roll-over rights were modeled.

### **III.D. Transmission Reliability Margin**

NERC defines Transmission Reliability Margin as:

*The amount of transmission transfer capability necessary to provide reasonable assurance that the interconnected transmission network will be secure. TRM accounts for the inherent uncertainty in system conditions and the need for operating flexibility to ensure reliable system operation as system conditions change.*

DEP's reliability planning studies model all confirmed transmission obligations for its BAA in its base case. Included in this is TRM for use by all LSEs. TRM is composed of contracted VACAR reserve sharing and inrush impacts. DEP models TRM by scheduling the reserved amount on actual reserved interfaces as posted on the DEP Open Access Same-time Information System ("OASIS").

In the planning horizon, DEC ensures VACAR reserve sharing requirements can be met through decrementing Total Transfer Capability ("TTC") by the TRM value required on each interface. Sufficient TRM is maintained on all DEC-VACAR interfaces to allow both export and import of the required VACAR reserves. DEC posts the TRM value for each interface on the DEC OASIS.

Both DEP and DEC ensure that TRM is maintained consistent with NERC requirements. The major difference between the methodologies used in planning by the two companies to calculate TRM is that DEP uses a flow-based methodology, while DEC decrements previously calculated TTC values on each interface.

### **III.E. Technical Analysis and Study Results**

Contingency screenings on the base case and scenarios were performed using Power System Simulator for Engineering (“PSS/E”) power flow or equivalent. Each transmission planner simulated its own transmission and generation down contingencies on its own transmission system.

DEC created generator maintenance cases that assume a major unit is removed from service and the system is economically redispatched to make up for the loss of generation. Additionally, outages of transmission connected solar sites were evaluated by creating cases that reflected one of two assumptions: 1) individual solar site being unavailable or 2) a group of solar sites being unavailable. For the latter, engineering judgement was used to group sites in common geographic areas.

Generator maintenance cases were developed for the following units:

Allen 4	Allen 5	Bad Creek 1
Belews Creek 1	Catawba 1	Cliffside 5
Cliffside 6	Broad River 1	Mill Creek 1
Jocassee 1	Lee 3	Marshall 3
McGuire 1	McGuire 2	Nantahala
Oconee 1	Oconee 3	Buck CC
Dan River CC	Rowan CC	Rockingham 1
Thorpe	Lincoln 1	Lee CC
Broad River 1	Cleveland 1	Cherokee Co-gen

DEP created generation down cases which included the use of TRM, as discussed in Section III.D. DEP TRM cases model interchange to avoid netting against imports, thereby creating a worst-case import scenario. TRM cases were developed for the following units:

Brunswick 1	Robinson 2
Harris	Asheville CC1

To understand impacts on each other’s system, DEC and DEP have exchanged their transmission contingency and monitored elements files in order for each company to simulate the impact of the other company’s



contingencies on its own transmission system. In addition, each company coordinated generation adjustments to accurately reflect the impact of each company's generation patterns.

The technical analysis was performed in accordance with the study methodology. The results from the technical analysis for the DEC and DEP systems were shared with all Participants. Solutions of known issues within DEC and DEP were discussed. New or emerging issues identified in the 2020 Study were also discussed with all Participants so that all are aware of potential issues. Appropriate solutions were developed and tested.

The results of the technical analysis were discussed throughout the study area based on thermal loadings greater than 90% for base reliability, and greater than 80% for resource supply options and local economic studies to allow evaluation of project acceleration.

### ***III.F. Assessment and Problem Identification***

DEC and DEP performed an assessment in accordance with the methodology and criteria discussed earlier in this section of this report, with the analysis work shared by DEC and DEP. The reliability issues identified from the assessments of both the base reliability cases and the local economic study scenarios were documented and shared within the PWG. These results will be reviewed and discussed with the stakeholder group for feedback.

### ***III.G. Solution Development***

The 2020 Study performed by the PWG confirmed base reliability problems already identified (i) by DEC and DEP in company-specific planning studies performed individually by the transmission owners and (ii) by the 2019 Study. The PWG participated in the review of potential solution alternatives to the identified base reliability problems and to the issues identified in the resource supply option analysis. The solution alternatives were simulated using the same assumptions and criteria described in Sections III.A through III.E. DEC and DEP developed planning cost estimates and construction schedules for the solution alternatives.

### ***III.H. Selection of Preferred Reliability Solutions***

For the base reliability study, the PWG compared solution alternatives and selected the preferred solution, balancing cost, benefit and risk. The PWG selected a preferred set of transmission improvements that provide a reliable and cost-effective transmission solution to meet customers' needs while prudently managing the associated risks.

### ***III.I. Contrast NCTPC Report to Other Regional Transfer Assessments***

For both the DEC and DEP BAAs, the results of the PWG study are consistent with SERC Long-Term Working Group ("LTWG") studies performed for similar timeframes. LTWG studies have recently been performed for the 2025 summer timeframe. The limiting facilities identified in the PWG study of base reliability have been previously identified in the LTWG studies for similar scenarios. These limiting facilities have also been identified in the individual transmission owner's internal assessments required by NERC reliability standards.

## **IV. Base Reliability Study Results**

The 2020 Study verified that DEC and DEP have projects already planned to address reliability concerns for the near-term (5 year) and long-term (10 year) planning horizons. There were no unforeseen problems identified in the reliability studies performed on the base cases.

The 2020 Plan is detailed in Appendix B which identifies the new and updated projects planned with an estimated cost of greater than \$10 million. Projects in the 2020 Plan are those projects identified in the base reliability study. For each of these projects, Appendix B provides the project status, the estimated cost, the planned in-service date, and the estimated time to complete the project.

The total estimated cost for the 17 reliability projects included in the 2020 Plan is \$804 million as documented in Appendix B. This compares to the original 2019 Plan estimate of \$591 million for 14 reliability projects. In-service dates and cost estimates for some projects that are planned or underway have been revised

based on updated information. An update to the 2019 plan was provided in the 2020 mid-year update published in June 2020 with an updated cost estimate of \$632 million. See Appendix D for a detailed comparison of this year’s Plan to the updated 2019 Plan.

## V. Local Economic Planning Studies

In 2020, the PWG analyzed as part of the local economic planning studies, scenarios that examine the impacts of high load growth in the Union and Cabarrus County areas of North Carolina. The study assumed 5–6% growth at Union Power Cooperative (UPC) deliveries. Table 5 identifies the two issues that resulted from this high load scenario analysis within the applicable planning window. Multiple alternatives are being investigated to address these identified overload issues other than upgrading the transmission lines. DEC is actively exploring solutions for both of these issues and is engaging NCEMC and UPC in discussions related to determining to best alternatives and solutions.

**Table 5**  
**Local Economic Planning Study – High Load Scenario (2025/2030)**

<b><u>Network Facility</u></b>
Clear Creek 100 kV Line (Harrisburg Tie–Morning Star Tie)
Rocky River 100 kV Line (Monroe Main–Oakboro Tie)

## VI. Local Public Policy Study Results

The analysis of this public policy impact was not completed in time for inclusion in this report. The NC offshore wind study results will be provided in a separate report once the full analysis is completed in early 2021.

## VII. Collaborative Transmission Plan

The 2020 Plan includes 17 reliability projects with an estimated cost of \$10 million or more each. These projects are listed in Appendix B. The total estimated cost for these 17 reliability projects in the 2020 Plan is \$804 million. This compares to the original 2019 Plan estimate of \$591 million for 14 reliability projects. In-service dates and cost estimates for some projects that are planned or underway have been revised based on updated information. An update to the 2019 plan was provided in the 2020 mid-year update published in June 2020 with an updated cost estimate of \$632 million. See Appendix D for a detailed comparison of this year's Plan to the updated 2019 Plan. The list of major projects will continue to be modified on an ongoing basis as new improvements are identified through the NCTPC Process and projects are in-service or eliminated from the list. Appendix C provides a more detailed description of each project in the 2020 Plan and includes the following information:

- 1) Reliability Projects: Description of the project.
- 2) Issue Resolved: Specific driver for project.
- 3) Status: Status of development of the project as described below:
  - a. In-Service – Projects with this status are in-service.
  - b. Underway – Projects with this status range from the Transmission Owner having some money in its current year budget for the project to the Transmission Owner having completed some construction activities for the project.
  - c. Planned – Projects with this status do not have money in the Transmission Owner's current year budget and the project is subject to change.
  - d. Conceptual – Projects with this status are not Planned at this time but will continue to be evaluated as a potential project in the future.
  - e. Deferred – Projects with this status were identified in the 2019 Report and have been deferred beyond the end of the planning horizon based on the 2020 Study results.

- f. Removed - Project is cancelled and no longer in the plan.
  
- 4) Transmission Owner: Responsible equipment owner designated to design and implement the project.
  
- 5) Projected In-Service Date: The date the project is expected to be placed in service.
  
- 6) Estimated Cost: The estimated cost, in nominal dollars, which reflects the sum of the estimated annual cash flows over the expected development period for the specific project (typically 2 – 5 years), including direct costs, loadings and overheads; but not including AFUDC. Each year's cash flow is escalated to the year of the expenditures. The sum of the expected cash flows is the estimated cost.
  
- 7) Project lead time: Number of years needed to complete project. For projects with the status of Underway, the project lead time is the time remaining to complete construction of the project and place the project in service.

# Appendix A

## Interchange Tables

**2025 SUMMER PEAK, 2025/2026 WINTER PEAK, 2030 SUMMER PEAK  
DUKE ENERGY CAROLINAS  
DETAILED INTERCHANGE (BASE)**

**Duke Energy Carolinas Modeled Imports – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
CPLC (NCEMC)	45	45	45
CPLC (NCEMC–Hamlet)	165	165	165
PJM (DVP/PJM)	2	2	2
SCEG (Chappells)	2	2	2
SCPSA (PMPA)	219	104	242
SCPSA (Seneca)	25	19	26
SEPA (Hartwell)	180	180	180
SEPA (Thurmond)	113	113	113
SOCO (EU)	231	0	0
SOCO (NCEMC)	44	44	44
<b>Total</b>	<b>1026</b>	<b>674</b>	<b>819</b>

**Duke Energy Carolinas Modeled Exports – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
CPLC (Broad River)	850	850	850
CPLC (NCEMC–Catawba)	307	307	307
CPLC (CPLC)	253	25	0
PJM (NCEMC–Catawba)	100	100	100
SCPSA (Haile)	15	15	15
<b>Total</b>	<b>1525</b>	<b>1297</b>	<b>1272</b>

**Duke Energy Carolinas Net Interchange – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
	<b>499</b>	<b>623</b>	<b>453</b>

Note: Positive net interchange indicates an export and negative interchange an import.

**2025 SUMMER PEAK, 2025/2026 WINTER PEAK, 2030 SUMMER PEAK  
DUKE ENERGY PROGRESS (EAST)  
DETAILED INTERCHANGE (BASE)**

**Duke Energy Progress (East) Modeled Imports – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
PJM (NCEMC–AEP)	100	100	100
PJM (NCEMC)	75	75	75
DUK (Broad River)	850	850	850
DUK (NCEMC–Catawba)	307	307	307
DUK (CPLC)	253	25	0
PJM (SEPA–KERR)	95	95	95
<b>Total</b>	<b>1680</b>	<b>1452</b>	<b>1427</b>

**Duke Energy Progress (East) Modeled Exports – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
CPLW (Transfer)	0	150	0
PJM (NCEMC–Hamlet)	165	165	165
DUK (NCEMC)	45	45	45
DUK (NCEMC–Hamlet)	165	165	165
<b>Total</b>	<b>375</b>	<b>525</b>	<b>375</b>

**Duke Energy Progress (East) Net Interchange – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
	<b>-1305</b>	<b>-927</b>	<b>-1052</b>

Note: Positive net interchange indicates an export and negative interchange an import.



**2025 SUMMER PEAK, 2025/2026 WINTER PEAK, 2030 SUMMER PEAK  
DUKE ENERGY PROGRESS (WEST)  
DETAILED INTERCHANGE (BASE)**

**Duke Energy Progress (West) Modeled Imports – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
CPLE (Transfer)	0	150	0
SCPSA (Waynesville)	22	22	22
TVA (SEPA)	14	14	14
<b>Total</b>	<b>36</b>	<b>186</b>	<b>36</b>

**Duke Energy Progress (West) Modeled Exports – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
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<b>Total</b>	---	---	---

**Duke Energy Progress (West) Net Interchange – MW**

	<b>25S</b>	<b>25/26W</b>	<b>30s</b>
	<b>-36</b>	<b>-186</b>	<b>-36</b>

Note: Positive net interchange indicates an export and negative interchange an import.

**2025 SUMMER PEAK, 2025/2026 WINTER PEAK, 2030 SUMMER PEAK DUKE ENERGY  
DUKE ENERGY PROGRESS (WEST), DUKE ENERGY PROGRESS (EAST)  
DETAILED INTERCHANGE (TRM)**

**Duke Energy Progress (West) Modeled Imports – MW**

	<b>25S, 25/26W, 30S</b>
AEP (TRM)	69
DUK (TRM)	191
TVA (TRM)	20
<b>Total</b>	<b>280</b>

**Duke Energy Progress (East) Modeled Imports – MW**

	<b>25S, 25/26W, 30S</b>
AEP (TRM)	100
DUK (TRM)	773
DVP (TRM)	427
SCEG (TRM)	200
SCPSA (TRM)	326
<b>Total</b>	<b>1826</b>

Note: Imports and exports for TRM are in addition to Base transfers



# **Appendix B**

## **Transmission Plan**

### **Major Project**

#### **Listings –**

# **Reliability Projects**



2020 Collaborative Transmission Plan – Reliability Projects (Estimated Cost > \$10M)						
Items identified in red are changes from the previous report.						
Project ID	Reliability Project	Status <sup>1</sup>	Transmission Owner	Projected In-Service Date	Estimated Cost (\$M) <sup>2</sup>	Project Lead Time (Years) <sup>3</sup>
0024	Durham–RTP 230 kV Line, Reconductor	Conceptual	DEP	TBD	20	4
0028	Brunswick #1–Jacksonville 230 kV Line, Loop into Folkstone 230 kV Substation	Removed	DEP	–	–	–
0031	Jacksonville–Grants Creek 230 kV Line and Grants Creek 230/115 kV Substation	In-service	DEP	6/1/2020	72	–
0032	Newport–Harlowe 230 kV Line, Newport SS and Harlowe 230/115 kV Substation	In-service	DEP	6/1/2020	55	–
0034	Sutton–Castle Hayne 115 kV North Line, Rebuild	Underway	DEP	6/1/2021	30	0.5



<b>2020 Collaborative Transmission Plan – Reliability Projects (Estimated Cost &gt; \$10M)</b> <b>Items identified in red are changes from the previous report.</b>						
Project ID	Reliability Project	Status <sup>1</sup>	Transmission Owner	Projected In-Service Date	Estimated Cost (\$M) <sup>2</sup>	Project Lead Time (Years) <sup>3</sup>
0039	Asheboro–Asheboro East 115 kV North Line, Reconductor	Underway	DEP	6/1/2022	24	1.5
0042	Rural Hall 100 kV, Install SVC	In-service	DEC	3/17/2020	44	–
0043	Orchard Tie 230/100 kV Tie Station, Construct	In-service	DEC	8/26/2020	104	–
0046	Windmere 100 kV Line (Dan River-Sadler), Construct	Underway	DEC	8/1/2023	26	2.5



2020 Collaborative Transmission Plan – Reliability Projects (Estimated Cost > \$10M)

Items identified in red are changes from the previous report.

Project ID	Reliability Project	Status <sup>1</sup>	Transmission Owner	Projected In-Service Date	Estimated Cost (\$M) <sup>2</sup>	Project Lead Time (Years) <sup>3</sup>
0048	Wilkes 230/100 kV Tie Station, Construct	Underway	DEC	6/1/2024	69	3
0050	Craggy–Enka 230 kV Line, Construct	Conceptual	DEP	12/1/2026	80	4
0051	Cokesbury 100 kV Line (Coronaca–Hodges), Upgrade	Planned	DEC	12/1/2024	16	3
0052	South Point Switching Station	Planned	DEC	12/1/2024	110	4
0053	Wateree 115 kV Plant, Upgrade 115/100 kV Transformers	Underway	DEP	12/1/2022	12	2



2020 Collaborative Transmission Plan – Reliability Projects (Estimated Cost > \$10M)						
Items identified in red are changes from the previous report.						
Project ID	Reliability Project	Status <sup>1</sup>	Transmission Owner	Projected In-Service Date	Estimated Cost (\$M) <sup>2</sup>	Project Lead Time (Years) <sup>3</sup>
0054	Carthage 230/115 kV Substation, Construct Sub	Conceptual	DEP	12/1/2027	15	4
0055	Falls 230 kV Sub, Add 300 MVAR SVC	Conceptual	DEP	12/1/2028	50	4
0056	Castle Hayne–Folkstone 115 kV Line, Rebuild	Conceptual	DEP	12/1/2028	52	4
0057	Holly Ridge North 115 kV Switching Station, Construct	Conceptual	DEP	12/1/2028	25	4
TOTAL					804	

<sup>1</sup> Status: **In-service**: Projects with this status are in-service. This status was updated as of 12/1/2020.

**Underway**: Projects with this status range from the Transmission Owner having some money in its current year budget for the project to the Transmission Owner having completed some construction activities for the project.



**Planned:** Projects with this status do not have money in the Transmission Owner’s current year budget; and the project is subject to change.

**Conceptual:** Projects with this status are not *planned* at this time but will continue to be evaluated as a potential project in the future.

**Deferred:** Projects with this status were identified in the 2019 Report and have been deferred beyond the end of the planning horizon based on analysis performed to develop the 2020 Collaborative Transmission Plan.

**Removed:** Project is cancelled and no longer in the plan

<sup>2</sup> The estimated cost is in nominal dollars which reflects the sum of the estimated annual cash flows over the expected development period for the specific project (typically 2 – 5 years), including direct costs, loadings and overheads; but not including AFUDC. Each year’s cash flow is escalated to the year of the expenditures. The sum of the expected cash flows is the estimated cost.

<sup>3</sup> For projects with a status of Underway, the project lead time is the time remaining to complete construction and place in-service.





# **Appendix C**

## **Transmission Plan**

### **Major Project**

#### **Descriptions –**

# **Reliability Projects**



## Table of Contents

<b><u>Project ID</u></b>	<b><u>Project Name</u></b>	<b><u>Page</u></b>
0024	Durham-RTP 230 kV Line, Reconductor	C-1
0031	Jacksonville-Grants Creek 230 kV Line and Grants Creek 230/115 kV Substation	C-2
0032	Newport-Harlowe 230 kV Line, Newport SS and Harlowe 230/115 kV Substation	C-3
0034	Sutton-Castle Hayne 115 kV North Line, Rebuild	C-4
0039	Asheboro-Asheboro East 115 kV North Line, Reconductor	C-5
0042	Rural Hall 100 kV, Install SVC	C-6
0043	Orchard Tie 230/100 kV Tie Station, Construct	C-7
0046	Windmere 100 kV Line (Dan River-Sadler), Construct	C-8
0048	Wilkes 230/100 kV Tie Station, Construct	C-9
0050	Craggy-Enka 230 kV Line, Construct	C-10
0051	Cokesbury 100 kV Line (Coronaca-Hodges), Upgrade	C-11
0052	South Point Switching Station	C-12
0053	Wateree 115 kV Plant, Upgrade 115/100 kV Transformers	C-13
0054	Carthage 230/115 kV Substation, Construct Sub	C-14
0055	Falls 230 kV Sub, Add 300 MVAR SVC	C-15
0056	Castle Hayne-Folkstone 115 kV Line, Rebuild	C-16
0057	Holly Ridge North 115 kV Switching Station, Construct	C-17

Note: The estimated cost for each of the projects described in Appendix C is in nominal dollars which reflects the sum of the estimated annual cash flows over the expected development period for the specific project (typically 2 – 5 years), including direct costs, loadings and overheads; but not including AFUDC. Each year's cash flow is escalated to the year of the expenditures. The sum of the expected cash flows is the estimated cost.



### Project ID and Name: 0024 – Durham–RTP 230 kV Line, Reconductor

<b>Project Description</b>
Reconductor approximately 10 miles of 230 kV line with 6–1590 ACSR conductor.

<b>Status</b>	Conceptual
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	TBD
<b>Estimated Time to Complete</b>	4 years
<b>Estimated Cost</b>	\$20 M

<b>Narrative Description of the Need for this Project</b>
With Harris Plant down, a common tower outage of the Method (DEC)–East Durham and the Durham–Method 230 kV Lines will cause an overload of the Durham 500 kV Sub-RTP 230 kV Switching Station Line.

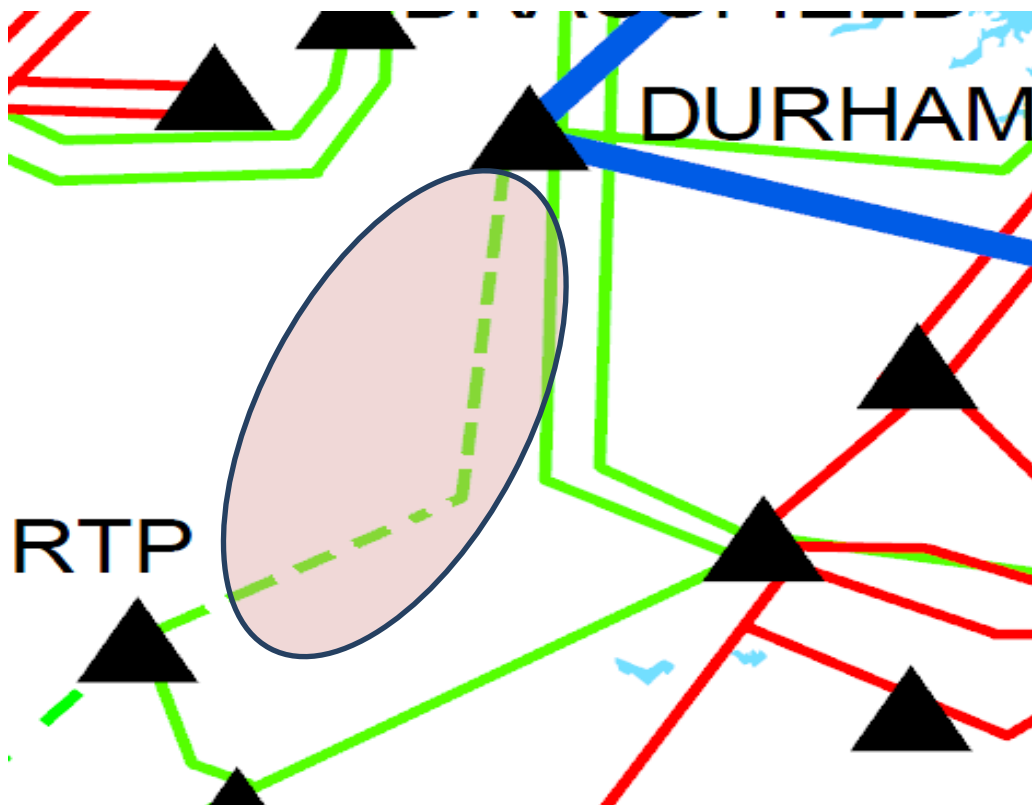
<b>Other Transmission Solutions Considered</b>
Construct a new line between Durham and RTP 230 kV subs.

<b>Why this Project was Selected as the Preferred Solution</b>
Cost and feasibility. Reconductoring is much more cost effective.



## Durham–RTP 230 kV Line

- **NERC Category P3 Violation**
- **Problem:** With Harris Plant down, a common tower outage of the Method (DEC)–East Durham and the Durham–Method 230 kV Lines will cause an overload of the Durham 500 kV Sub-RTP 230 kV Switching Station Line.
- **Solution:** Reconductor approximately 10 miles of 230 kV line with 6-1590 ACSR conductor.





### Project ID and Name: 0031 – Jacksonville–Grants Creek 230 kV Line and Grants Creek 230/115 kV Substation

<b>Project Description</b>
The project scope consists of constructing a new 230 kV Line from Jacksonville 230 kV to a new 230 kV substation in the Grants Creek area. The 230 kV line shall be constructed with 6-1590 MCM ACSR or equivalent and will convert the existing Jacksonville–Havelock 230 kV Line into Jacksonville–Grants Creek 230 kV Line and Grants Creek–Havelock 230 kV Line. The new 230 kV Grants Creek Substation will be built with 4-230 kV breakers, a new 230/115 kV transformer, and tap into the Jacksonville City–Harmon POD 115 kV Feeder with 1-115 kV breaker.

<b>Status</b>	<b>In-service</b>
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	6/1/2020
<b>Estimated Time to Complete</b>	Completed
<b>Estimated Cost</b>	\$72 M

<b>Narrative Description of the Need for this Project</b>
The common tower outage of Jacksonville – Havelock 230 kV Line and Jacksonville – Jacksonville City 115 kV Line may cause the voltages in the Camp Lejeune area to fall below the planning criteria. Also, outage of the Jacksonville–New Bern 230 kV Line may cause the Havelock–Jacksonville 230 kV to overload.

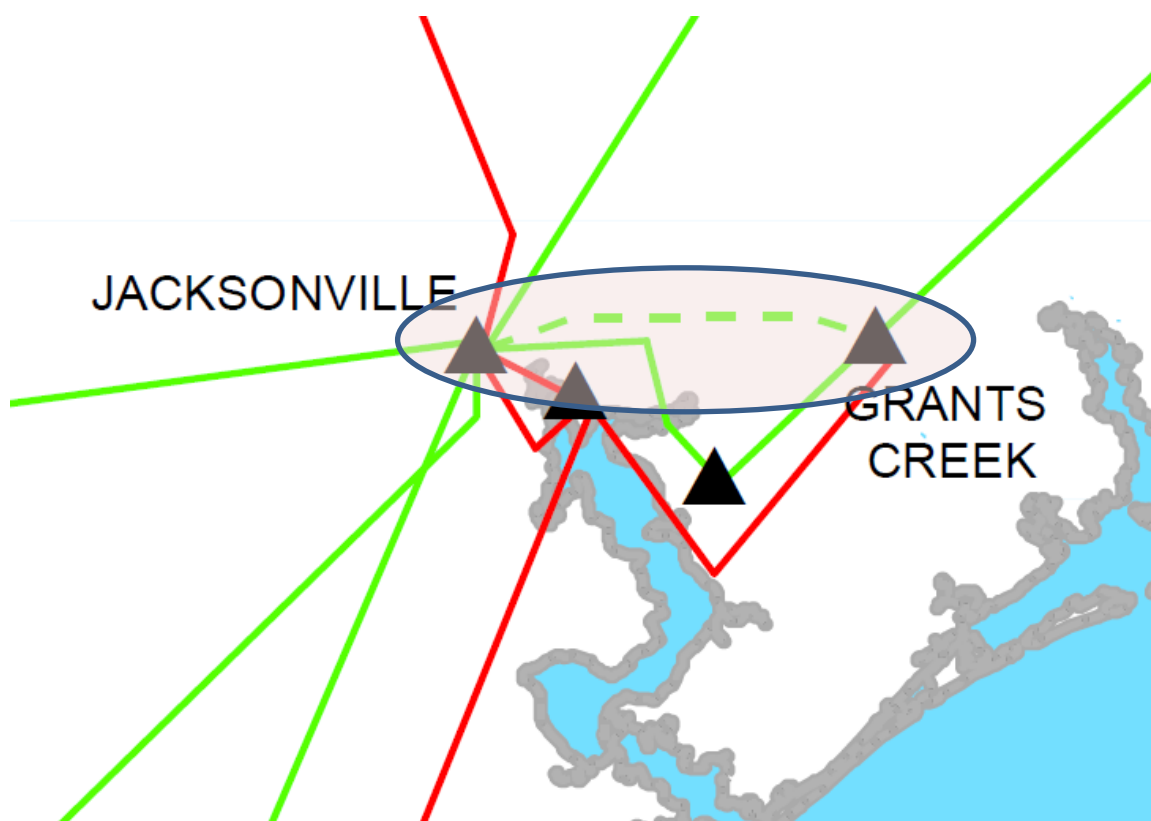
<b>Other Transmission Solutions Considered</b>
Construct 230 kV feeder from Jacksonville to Camp Lejeune Tap.

<b>Why this Project was Selected as the Preferred Solution</b>
The alternate solution was determined to be infeasible due to routing challenges.



## Jacksonville–Grants Creek 230 kV Line and Grants Creek 230/115 kV Substation

- **NERC Category P7 violation**
- **Problem:** The common tower outage of Jacksonville – Havelock 230 kV Line and Jacksonville – Jacksonville City 115 kV Line may cause the voltages in the Camp Lejeune area to fall below the planning criteria. Also, outage of the Jacksonville–New Bern 230 kV Line may cause the Havelock–Jacksonville 230 kV Line to overload.
- **Solution:** Construct new 230 kV line and substation.





### Project ID and Name: 0032 – Newport–Harlowe 230 kV Line, Newport SS and Harlowe 230/115 kV Substation

<b>Project Description</b>
Construct new 230 kV Switching Station in the Newport Area, construct new 230 kV Substation in the Harlowe Area, and construct the Newport Area–Harlowe Area 230 kV line comprised of 3-1590 MCM ACSR or equivalent. The Newport Area 230 kV Switching Station will initially consist of a 3-breaker ring bus but should be laid out for future development as a standard 230/115 kV substation with breaker-and-a-half configuration in the 230 kV yard. The Harlowe Area 230 kV Substation will initially consist of one 200 MVA (or 300MVA), 230/115 kV transformer and 3-115 kV breakers, and should be laid out for future development as a standard 230/115 kV substation with breaker-and-a-half configuration in the 230 kV yard.

<b>Status</b>	<b>In-service</b>
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	6/1/2020
<b>Estimated Time to Complete</b>	Completed
<b>Estimated Cost</b>	\$55 M

<b>Narrative Description of the Need for this Project</b>
By summer 2020, an outage of the Havelock terminal of the Havelock–Morehead Wildwood 115 kV North Line will cause the voltages in the Havelock area to fall below planning criteria. The construction of this new line will mitigate this voltage problem.

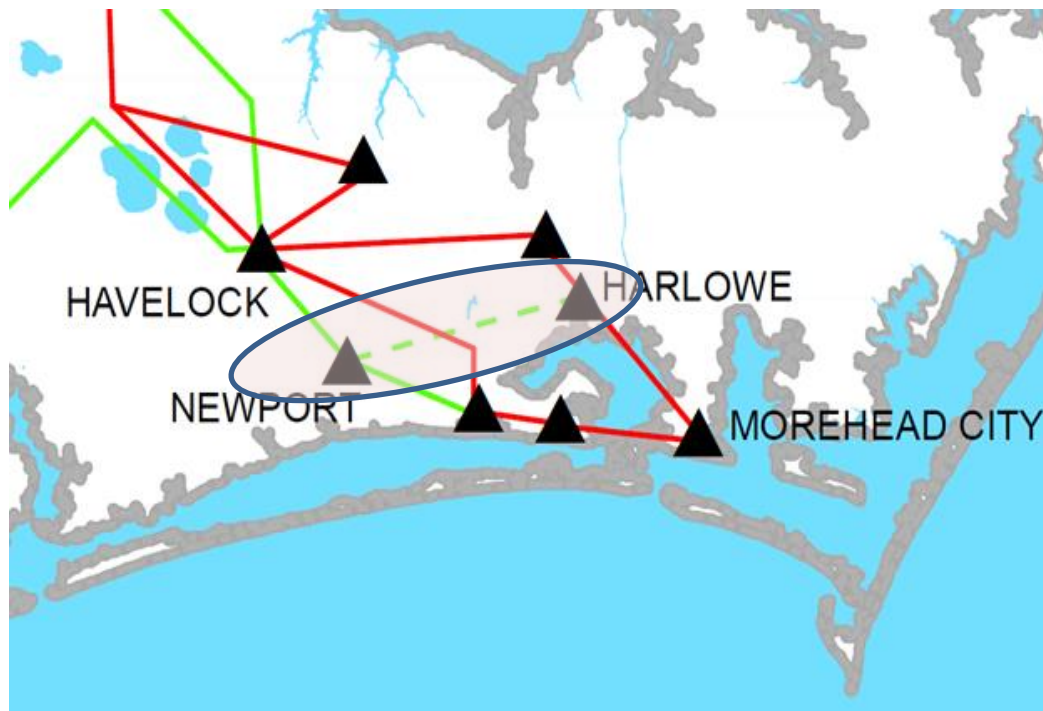
<b>Other Transmission Solutions Considered</b>
Convert Havelock–Morehead Wildwood 115 kV North Line to 230 kV.

<b>Why this Project was Selected as the Preferred Solution</b>
The cost and construction feasibility are much better with selected alternative.



## **Newport–Harlowe 230 kV Line, Newport SS and Harlowe 230/115 kV Substation**

- **NERC Category P1 violation**
- **Problem:** By summer 2020, an outage of the Havelock terminal of the Havelock–Morehead Wildwood 115 kV North Line will cause the voltages in the Havelock area to fall below planning criteria. The construction of this new line will mitigate this voltage problem.
- **Solution:** Construct new 230 kV line, switching station and substation.







### Project ID and Name: 0034 – Sutton–Castle Hayne 115 kV North Line, Rebuild

<b>Project Description</b>
This project consists of rebuilding the Sutton Plant – Castle Hayne 115 kV North Line using 1272 MCM ACSR conductor or equivalent (approximately 8 miles). The line traps at both Sutton and Castle Hayne terminals will be removed in conjunction with the installation of OPGW. The 800 A current transformers at both line terminals will have to be updated as part of this project.

<b>Status</b>	Underway
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	6/1/2021
<b>Estimated Time to Complete</b>	0.5 years
<b>Estimated Cost</b>	\$30 M

<b>Narrative Description of the Need for this Project</b>
By 2021, with all area generation online, the loss of the Sutton Plant–Castle Hayne 115 kV South Line will cause the Sutton Plant–Castle Hayne 115 kV North Line to exceed its thermal rating.

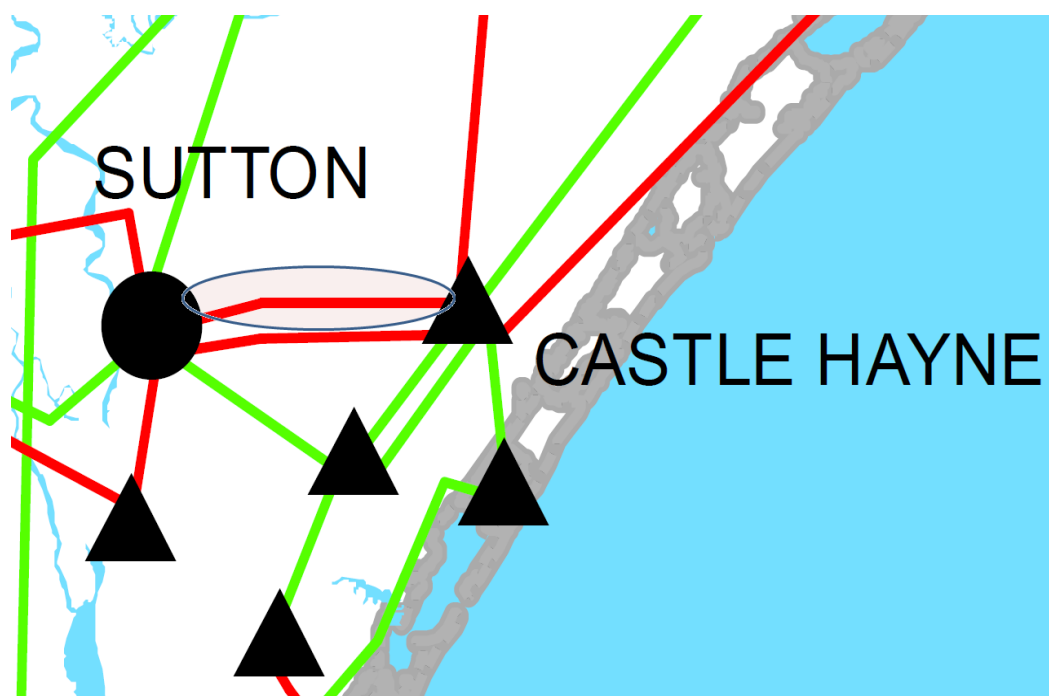
<b>Other Transmission Solutions Considered</b>
Convert 115 kV line to 230 kV.

<b>Why this Project was Selected as the Preferred Solution</b>
Cost and feasibility are much improved with selected alternative.



## Sutton–Castle Hayne 115 kV North Line, Rebuild

- **NERC Category P1 violation**
- **Problem:** By 2021, with all area generation online, the loss of the Sutton Plant–Castle Hayne 115 kV South Line will cause the Sutton Plant–Castle Hayne 115 kV North Line to exceed its thermal rating.
- **Solution:** Rebuild 115 kV line.





### Project ID and Name: 0039 – Asheboro–Asheboro East 115 kV North Line, Reconductor

<b>Project Description</b>
This project consists of rebuilding/reconductoring approximately 6.5 miles of the existing 115 kV line using 3-1590 or equivalent conductor. This project requires the replacement of disconnect switches at Asheboro 230 kV and the replacement of the breaker, the disconnect switches, and the 115 kV east bus at Asheboro East 115 kV associated with this line. Both ends of the line will also require CT/metering equipment upgrades such that they are not the limit to the line rating. The upgraded equipment for this line should be 2000 amp minimum.

<b>Status</b>	Underway
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	6/1/2022
<b>Estimated Time to Complete</b>	1.5 years
<b>Estimated Cost</b>	\$24 M

<b>Narrative Description of the Need for this Project</b>
This project is needed to alleviate loading on the Asheboro–Asheboro East 115 kV North line under the contingency of losing the Asheboro–Asheboro East 115 kV South line with Harris Plant down.

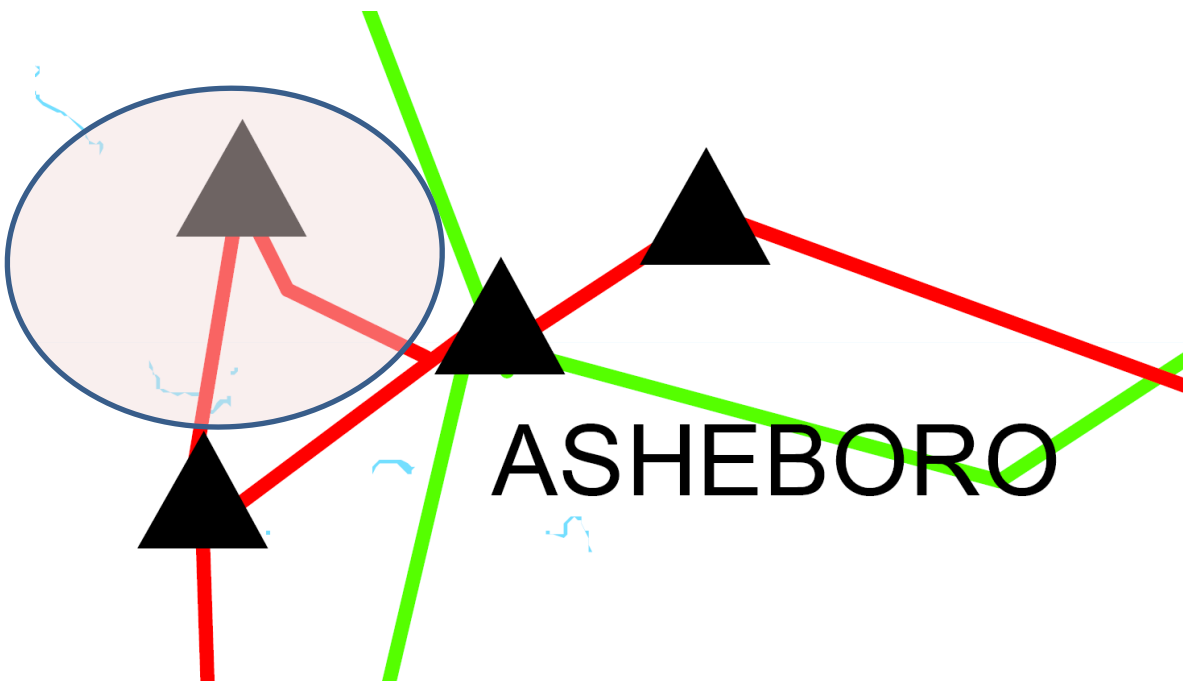
<b>Other Transmission Solutions Considered</b>
Construct a new 115 kV line from Asheboro to Asheboro East.

<b>Why this Project was Selected as the Preferred Solution</b>
Cost and feasibility.



## Asheboro–Asheboro East 115 kV North Line, Reconductor

- **NERC Category P3 violation**
- **Problem:** By the summer of 2020, with Harris down, the loss of the Asheboro–Asheboro East 115 kV South line will cause the Asheboro–Asheboro East 115 kV North line to overload.
- **Solution:** Rebuild/reconductor the Asheboro–Asheboro East 115 kV North Line and upgrade equipment.





### Project ID and Name: 0042 – Rural Hall 100 kV, Install SVC

<b>Project Description</b>
This project consists of installing a -100/+300 MVAR SVC at Rural Hall 100 kV.

<b>Status</b>	<b>In-service</b>
<b>Transmission Owner</b>	DEC
<b>Planned In-Service Date</b>	3/17/2020
<b>Estimated Time to Complete</b>	Completed
<b>Estimated Cost</b>	\$44 M

<b>Narrative Description of the Need for this Project</b>
Installation of an SVC at Rural Hall will mitigate dynamic voltage concerns driven by certain contingency conditions in DEC.

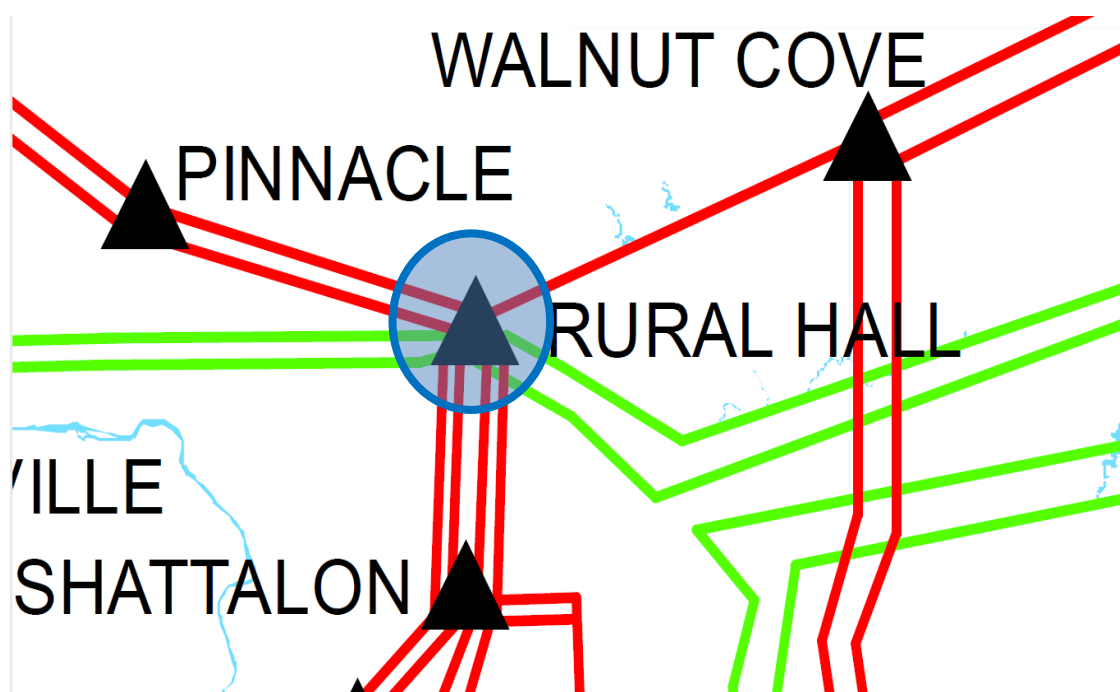
<b>Other Transmission Solutions Considered</b>
New generation.

<b>Why this Project was Selected as the Preferred Solution</b>
Solution can be implemented quicker than new generation and at a lower cost.



## Rural Hall 100 kV, Install SVC

- **Problem:** Under certain conditions, additional voltage support is required in order to maintain system reliability.
- **Solution:** The installation of an SVC at Rural Hall 100 kV will provide voltage support to the region and increase system reliability under certain conditions. As part of the project there will be a reconfiguration of the 100 kV capacitors at Rural Hall.





### Project ID and Name: 0043 – Orchard Tie 230/100 kV Tie Station, Construct

<b>Project Description</b>
This project consists of constructing the Orchard Tie 230/100 kV Tie Station

<b>Status</b>	In-Service
<b>Transmission Owner</b>	DEC
<b>Planned In-Service Date</b>	8/26/2020
<b>Estimated Time to Complete</b>	Completed
<b>Estimated Cost</b>	\$104 M

<b>Narrative Description of the Need for this Project</b>
The installation of this new 230/100 kV tie station will provide greater ability to meet local load growth and maintain compliance with NERC Transmission Planning Standards.

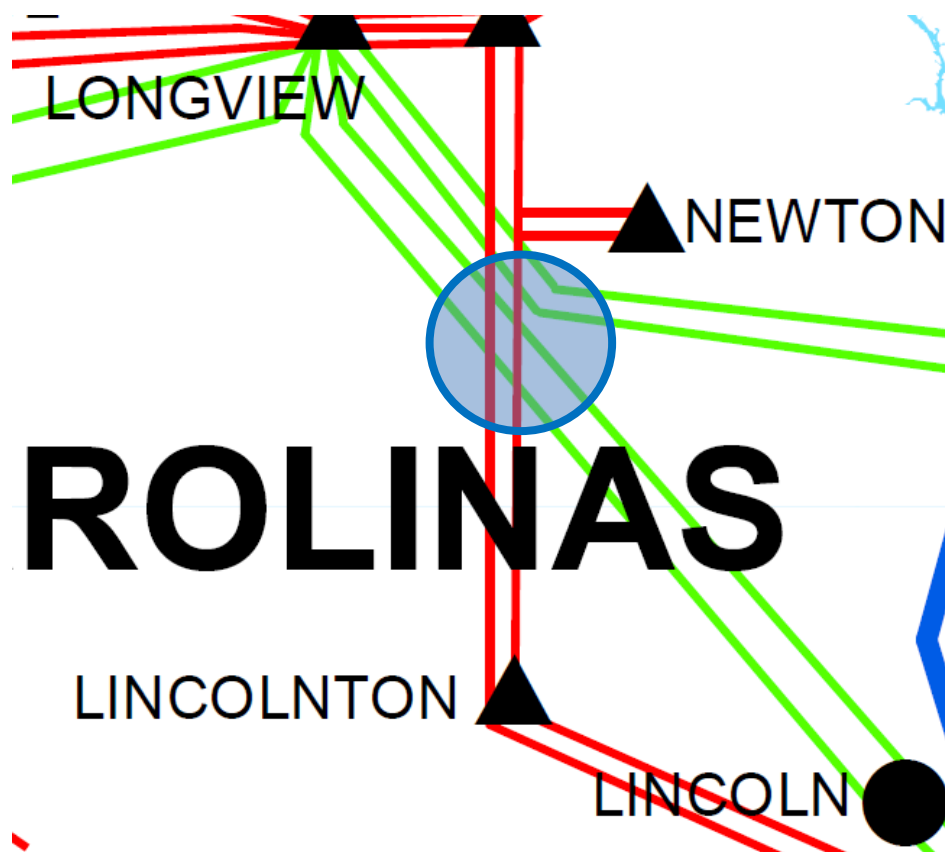
<b>Other Transmission Solutions Considered</b>
Upgrade ≈30 miles of 100 kV.

<b>Why this Project was Selected as the Preferred Solution</b>
Ability to meet local load growth and cost of rebuilding 100 kV line.



## Orchard Tie 230/100 kV Tie Station, Construct

- **Problem:** Existing transmission lines are not sufficient to meet local load growth.
- **Solution:** Fold-in existing 230 kV and 100 kV lines to new station. Add sufficient transformation between 230 kV and 100 kV.







### Project ID and Name: 0046 – Windmere 100 kV Line (Dan River–Sadler), Construct

<b>Project Description</b>
This project consists of building a new 100 kV line (954 AAC) along an existing ROW.

<b>Status</b>	Underway
<b>Transmission Owner</b>	DEC
<b>Planned In-Service Date</b>	8/1/2023
<b>Estimated Time to Complete</b>	2.5 years
<b>Estimated Cost</b>	\$26 M

<b>Narrative Description of the Need for this Project</b>
The Reidsville and Wolf Creek 100 kV lines (Dan River–Sadler) can become overloaded for the loss of any of the circuits between Dan River and Sadler.

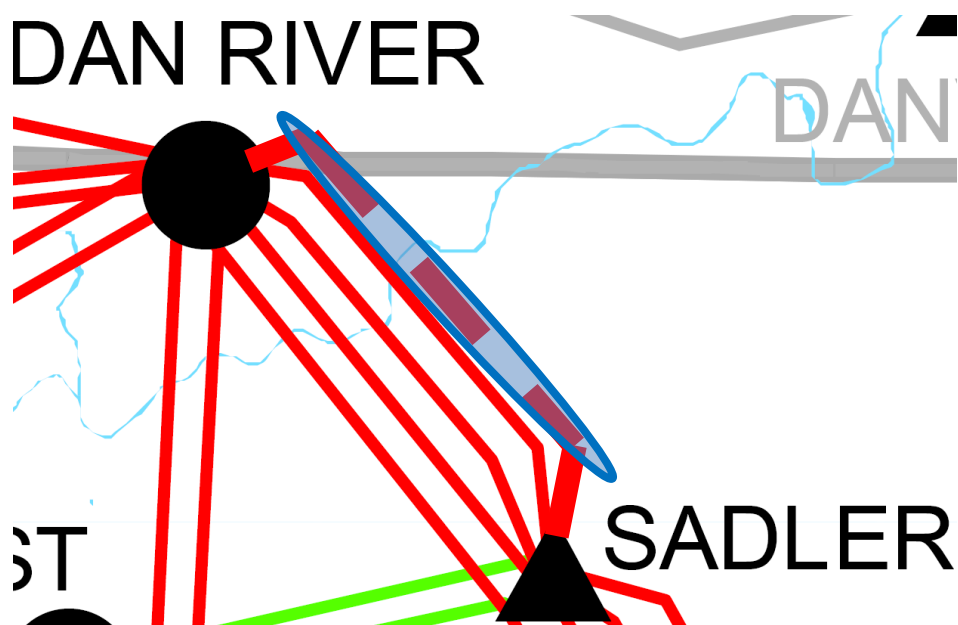
<b>Other Transmission Solutions Considered</b>
Rebuilding both double circuit 100 kV lines (≈8 miles each) between Dan River and Sadler.

<b>Why this Project was Selected as the Preferred Solution</b>
Greater operational flexibility in the area.



### Windmere 100 kV Line (Dan River–Sadler), Construct

- **NERC Category P3 violation**
- **Problem:** Loss of any of the four existing 100 kV circuits between Dan River and Sadler and can overload the remaining circuits.
- **Solution:** Construct new 100 kV line.





## Project ID and Name: 0048 – Wilkes 230/100 kV Tie Station, Construct

<b>Project Description</b>
This project consists of building a new 230/100 kV Wilkes tie station and re-routing local transmission lines.

<b>Status</b>	Underway
<b>Transmission Owner</b>	DEC
<b>Planned In-Service Date</b>	6/1/24
<b>Estimated Time to Complete</b>	3 years
<b>Estimated Cost</b>	\$69 M

<b>Narrative Description of the Need for this Project</b>
The primary driver for this project is to increase support in the area around Wilkesboro NC. Contingencies, especially in the winter, have the tendency to drop voltage in the area as well as some thermal loading concerns with the loss of the Oxford 100 kV line. The secondary driver is to alleviate the need to rebuild N Wilkesboro Tie as a result of the need to install a bus junction breaker at N Wilkesboro Tie. Presently, loss of the single N Wilkesboro bus takes out six 100 kV lines, causes loss of load and low voltage problems in the area. Installation of a bus junction breaker would also cause thermal loading issues requiring a line upgrade. This project also makes use of 230 kV transmission lines that pass adjacent to the new 230/100 kV tie station.

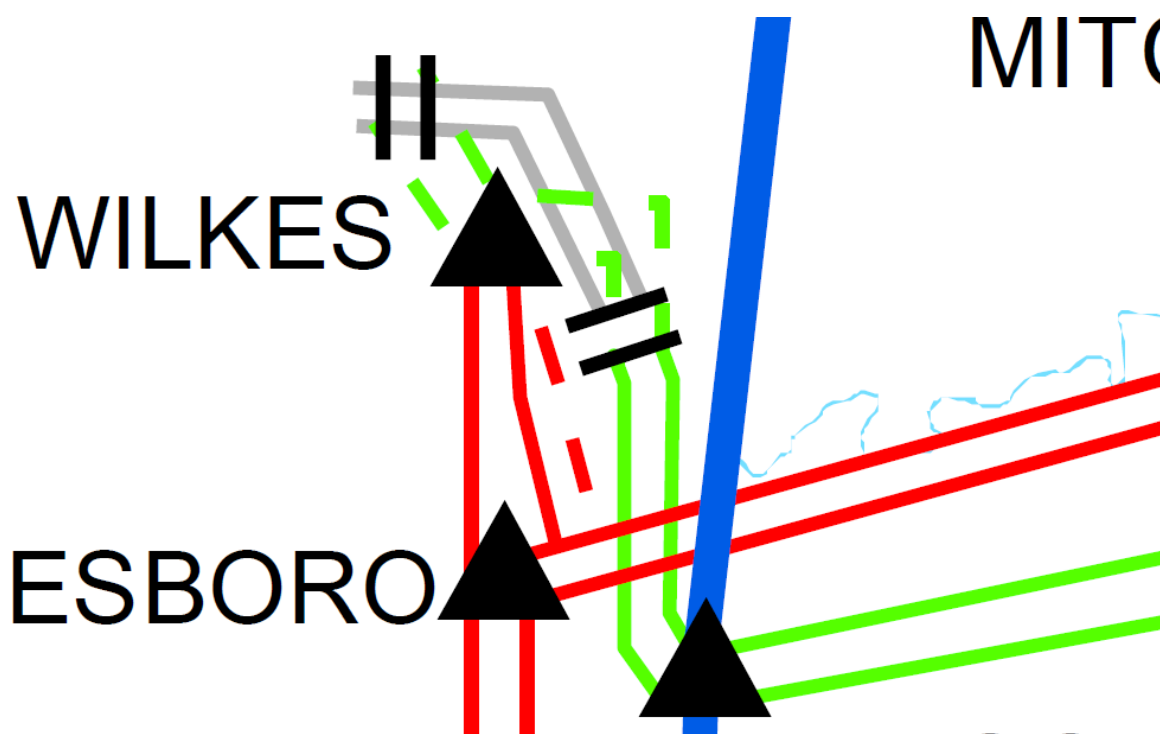
<b>Other Transmission Solutions Considered</b>
Rebuild N Wilkesboro Tie to allow installation of a bus tie breaker.

<b>Why this Project was Selected as the Preferred Solution</b>
Greater long term value to system and operational flexibility in the area.



### Wilkes 230/100 kV Tie Station, Construct

- **NERC Category P1, P2, & P3 violation**
- **Problem:** Contingency events in the Wilkesboro, NC area cause thermal loading issues, loss of load and low voltage problems in the area.
- **Solution:** Construct new 230/100 kV tie station.





### Project ID and Name: 0050 – Craggy-Enka 230 kV Line, Construct

<b>Project Description</b>
This project consists of constructing approximately 10 miles of new 230 kV transmission line between the Craggy and Enka Substations.

<b>Status</b>	Conceptual
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	12/1/2026
<b>Estimated Time to Complete</b>	4 years
<b>Estimated Cost</b>	\$80 M

<b>Narrative Description of the Need for this Project</b>
Opening the Asheville end of the Oteen 115 kV West line overloads the Enka – West Asheville 115 kV line. Also, a NERC P6 outage of Craggy–Enka 115 and Asheville–Oteen 115 West lines has no viable operating procedure beginning 12/1/2026. Outage of the West Asheville 115 kV bus overloads the Craggy–Enka 115 kV line.

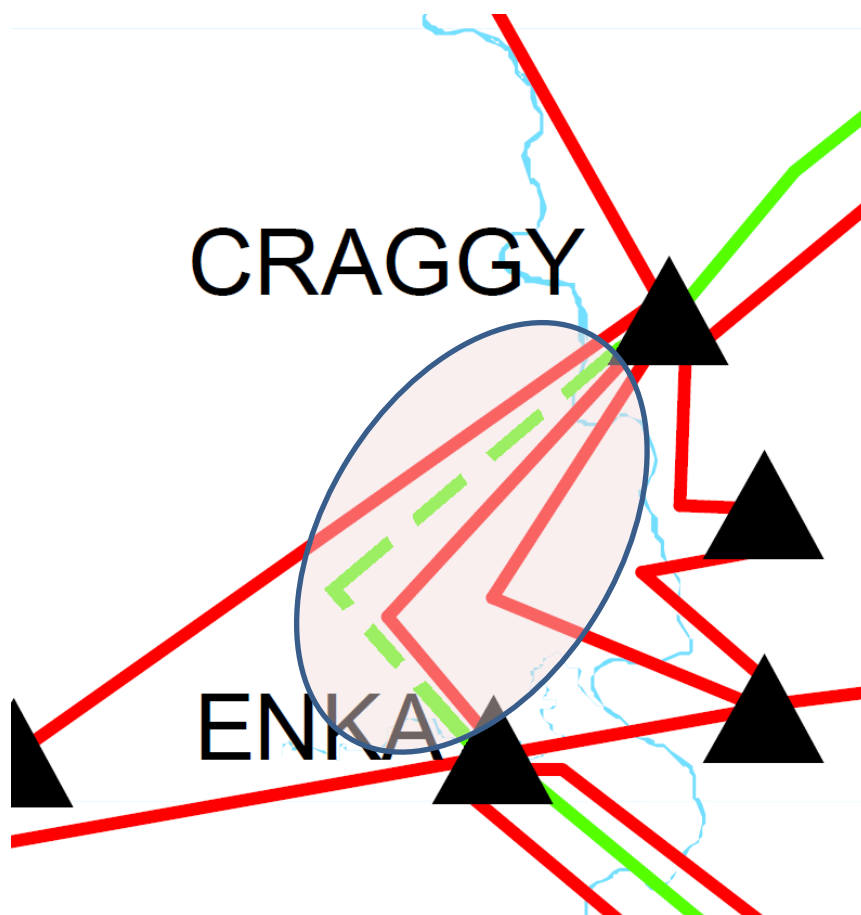
<b>Other Transmission Solutions Considered</b>
Reconductoring multiple transmission lines. These include the Enka–West Asheville 115 kV Line, the Craggy–Enka 115 kV line, the Canton–Craggy 115 kV Line, and the Asheville–Oteen 115 kV East Line.

<b>Why this Project was Selected as the Preferred Solution</b>
Cost and feasibility.



## Craggy–Enka 230 kV Line, Construct

- **NERC Category P3 & P6 violation**
- **Problem:** Opening the Asheville end of the Oteen 115 kV West line overloads the Enka – West Asheville 115 kV line. Also, a NERC P6 outage of Craggy–Enka 115 kV and Asheville–Oteen 115 kV West lines has no viable operating procedure beginning 12-2026. Outage of the West Asheville 115 kV bus overloads the Craggy–Enka 115 kV line.
- **Solution:** Construct the Craggy–Enka 230 kV Line.





### Project ID and Name: 0051 – Cokesbury 100 kV Line (Coronaca–Hodges), Upgrade

<b>Project Description</b>
This project consists of rebuilding 9.2 miles of the existing 477 ACSR conductor with 1272 ACSR.

<b>Status</b>	Planned
<b>Transmission Owner</b>	DEC
<b>Planned In-Service Date</b>	12/1/24
<b>Estimated Time to Complete</b>	3 years
<b>Estimated Cost</b>	\$16 M

<b>Narrative Description of the Need for this Project</b>
These lines may become overloaded for loss of one of the circuits.

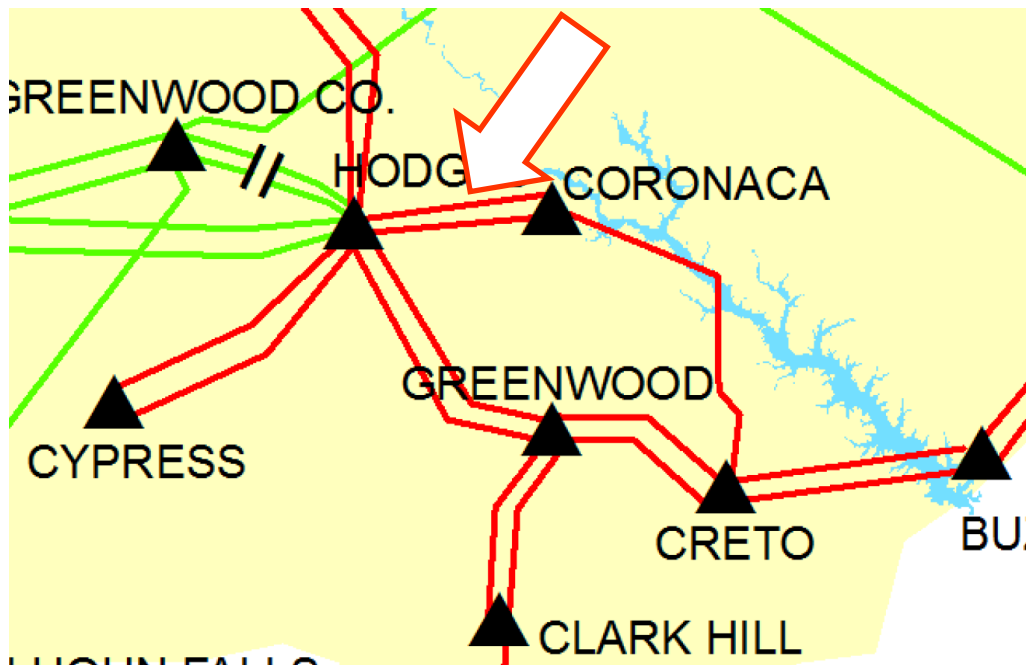
<b>Other Transmission Solutions Considered</b>
New transmission line(s).

<b>Why this Project was Selected as the Preferred Solution</b>
New transmission line(s) would require additional right-of-way, adding to the cost of the project.



### Cokesbury 100 kV Line (Coronaca–Hodges), Upgrade

- **NERC Category P3 violation**
- **Problem:** Loss of one of the Greenwood–Hodges 100 kV lines may overload the remaining line.
- **Solution:** Rebuild 100 kV lines with higher capacity conductors.







### Project ID and Name: 0052 – South Point Switching Station

<b>Project Description</b>
This project consists of replacing (in a new location) the switchyard at Allen Steam Station and upgrading the existing 230/100 kV transformers.

<b>Status</b>	Planned
<b>Transmission Owner</b>	DEC
<b>Planned In-Service Date</b>	6/1/24
<b>Estimated Time to Complete</b>	3 years
<b>Estimated Cost</b>	\$110 M

<b>Narrative Description of the Need for this Project</b>
The transformers may become overloaded for loss of the other transformer, and there are obsolescence issues with the existing switchyard at Allen Steam Station.

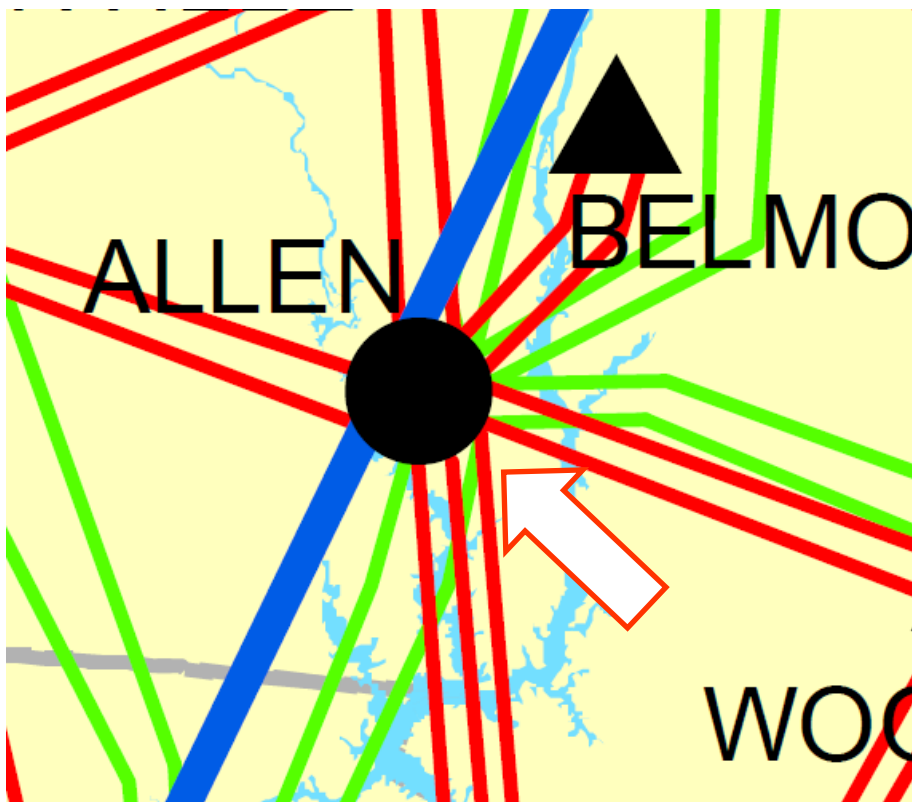
<b>Other Transmission Solutions Considered</b>
Convert Wylie Switching Station to 230/100 kV. Rebuild Allen Steam Station in its current location, and replace existing 230/100 kV transformers at Allen Steam Station.

<b>Why this Project was Selected as the Preferred Solution</b>
Cost and timing



### South Point Switching Station

- **NERC Category P3 Violation**
- **Problem:** Post-generation retirement at Allen Steam Station, loss of one 230/100 kV transformers at Allen may overload the remaining transformer.
- **Solution:** Upgrade to larger transformers





### Project ID and Name: 0053 – Wateree 115 kV Plant, Upgrade 115/100 kV Transformers

<b>Project Description</b>
This project consists of replacing the two existing 115/100 kV autotransformers at Wateree Plant with two new 168 MVA 115/100 kV autotransformers. While the two existing 115/100 kV Wateree transformers share a single breaker, the new transformers will be separately breakered so that either one can trip out with the other bank still transferring power between DEP and DEC. (The Wateree Plant is owned by DEC, but the existing 115/100 kV transformers and the 115 kV bus are owned by DEP.)

<b>Status</b>	Underway
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	12/1/2022
<b>Estimated Time to Complete</b>	2 years
<b>Estimated Cost</b>	\$12 M

<b>Narrative Description of the Need for this Project</b>
By winter 2022-23, the NERC P3 outage of Robinson Nuclear plus outage of either the Richmond–Newport 500 kV line or the Camden–Lugoff 230 kV line causes an overload of the existing Wateree 115/100 kV transformers. In addition, the existing Wateree 115/100 kV transformers have reached end of life based on analysis from Asset Management.

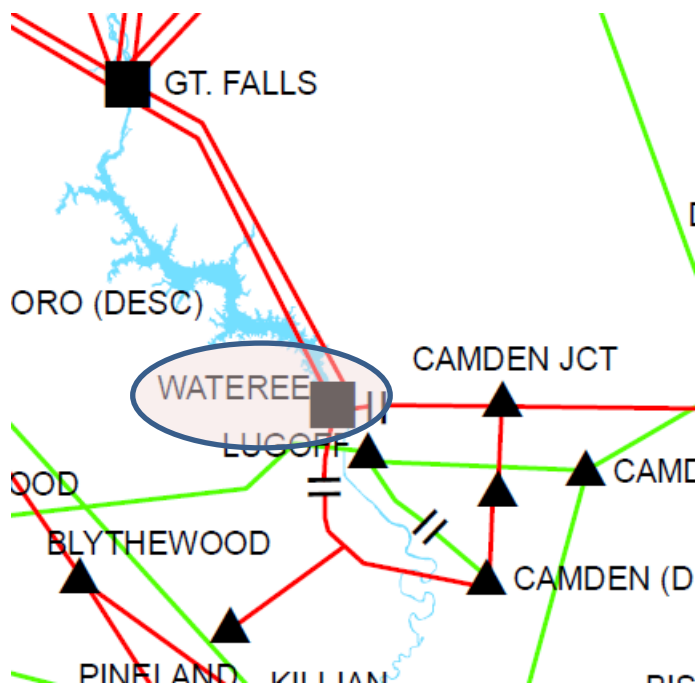
<b>Other Transmission Solutions Considered</b>
New transmission lines.

<b>Why this Project was Selected as the Preferred Solution</b>
The cost and construction feasibility are much better with selected alternative.



## Wateree 115 kV Plant, Upgrade 115/100 kV Transformers

- **NERC Category P3 violation**
- **Problem:** By winter 2022-23, the NERC P3 outage of Robinson Nuclear plus outage of either the Richmond–Newport 500 kV line or the Camden–Lugoff 230 kV line causes an overload of the existing Wateree 115/100 kV transformers. In addition, the existing Wateree 115/100 kV transformers have reached end of life based on analysis from Asset Management.
- **Solution:** Upgrade existing transformers.





### Project ID and Name: 0054 – Carthage 230/115 kV Substation, Construct Substation

<b>Project Description</b>
Construct a new 230/115 kV substation near the existing Carthage 115 kV substation. Loop in the existing Cape Fear–West End 230 kV line and West End–Southern Pines 115 kV feeder. The new Carthage 230–West End 115 kV line will be normally open at Carthage 230.kV.

<b>Status</b>	Conceptual
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	12/1/2027
<b>Estimated Time to Complete</b>	4 years
<b>Estimated Cost</b>	\$15 M

<b>Narrative Description of the Need for this Project</b>
By winter 2027-28, the NERC P1 outage of one West End transformer overloads the other and voltage at Southern Pines 115 kV drops below criteria.

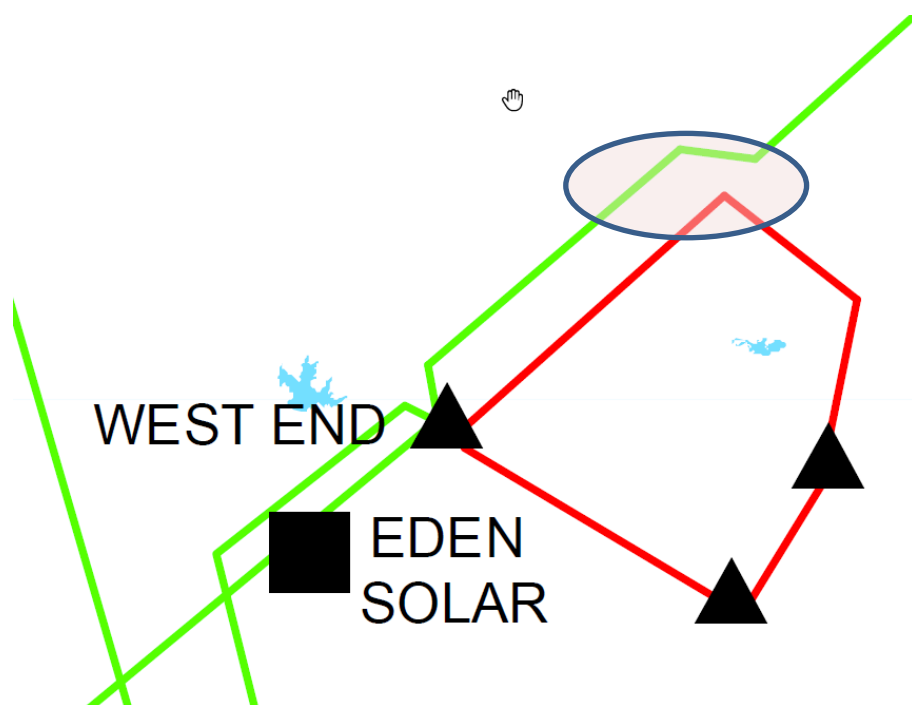
<b>Other Transmission Solutions Considered</b>
Convert several 115 kV substations to 230 kV.

<b>Why this Project was Selected as the Preferred Solution</b>
The cost and construction feasibility are much better with selected alternative.



## Carthage 230/115 kV Substation, Construct Substation

- **NERC Category P1 violation**
- **Problem:** By winter 2027-28, the NERC P1 outage of one West End transformer overloads the other and voltage at Southern Pines 115 kV drops below criteria.
- **Solution:** Construct new 230/115 kV substation in the Carthage area.





### Project ID and Name: 0055 – Falls 230 kV Sub, Add 300 MVAR SVC

<b>Project Description</b>
At Falls 230 kV Substation add a 300 MVAR 230 kV Static Var Compensator (SVC).

<b>Status</b>	Conceptual
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	12/1/2028
<b>Estimated Time to Complete</b>	4 years
<b>Estimated Cost</b>	\$50 M

<b>Narrative Description of the Need for this Project</b>
With the future retirement of Roxboro and Mayo plants, several DEP areas were observed to have significant contingency voltage depression.

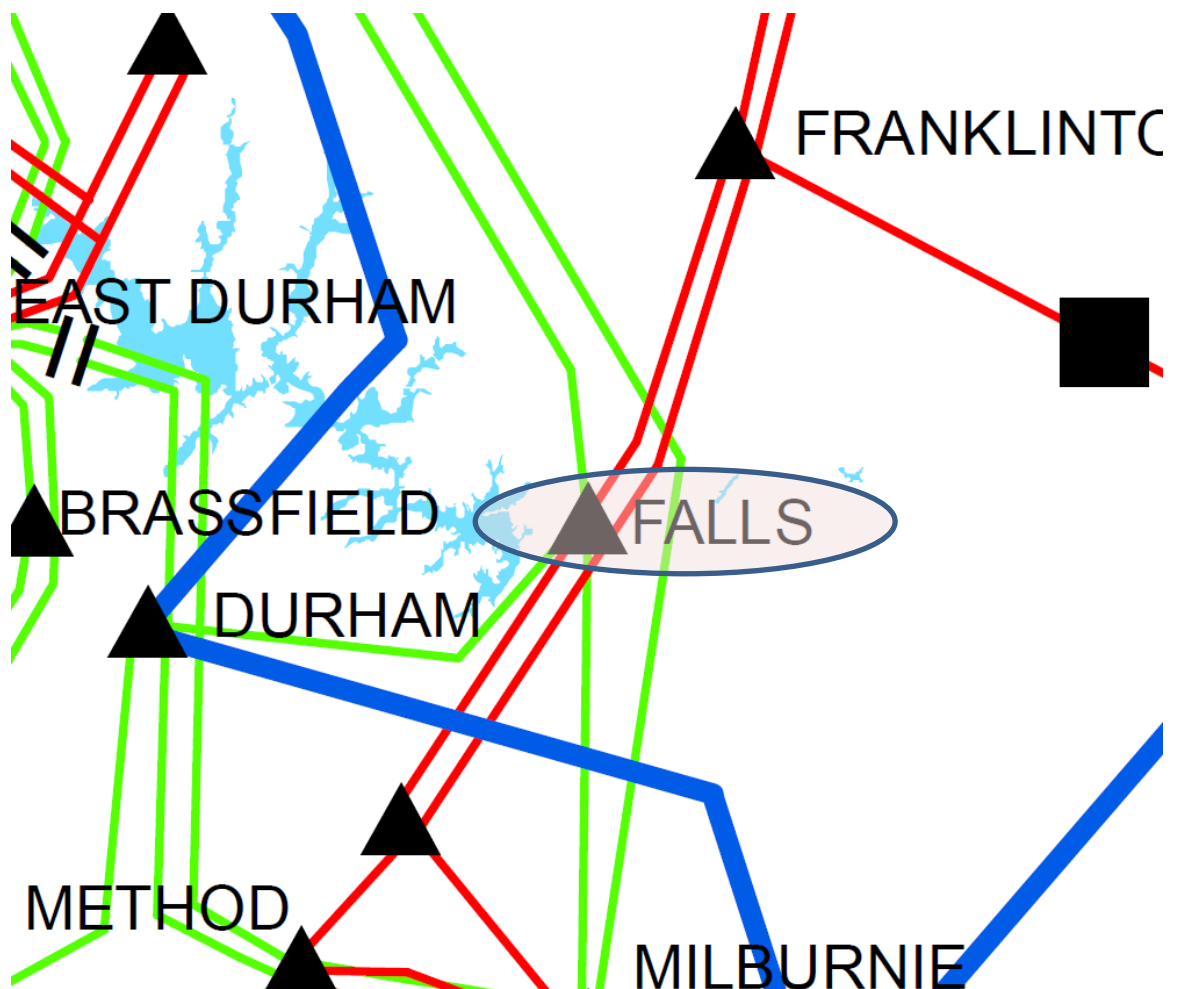
<b>Other Transmission Solutions Considered</b>
Replacement generation in the Roxboro area.

<b>Why this Project was Selected as the Preferred Solution</b>
The cost and construction feasibility are much better with selected alternative.



### Falls 230 kV Sub, Add 300 MVAR SVC

- **NERC Category P1 violation**
- **Problem:** With the future retirement of Roxboro and Mayo plants, several DEP areas were observed to have significant contingency voltage depression.
- **Solution:** Add 300 MVAR SVC at the Falls 230 kV Substation.







### Project ID and Name: 0056 – Castle Hayne–Folkstone 115 kV Line, Rebuild

<b>Project Description</b>
Rebuild approximately 25.91 miles of 115 kV line (Castle Hayne 230 kV Sub to structure #251) with 1272 MCM ACSR or equivalent.

<b>Status</b>	Conceptual
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	12/1/2028
<b>Estimated Time to Complete</b>	4 years
<b>Estimated Cost</b>	\$52 M

<b>Narrative Description of the Need for this Project</b>
By winter 2028/29, an outage of the Castle Hayne – Folkstone 230 kV line will cause the Castle Hayne 230 kV Sub-Folkstone 115 kV line to overload. This project will mitigate the overload problem.

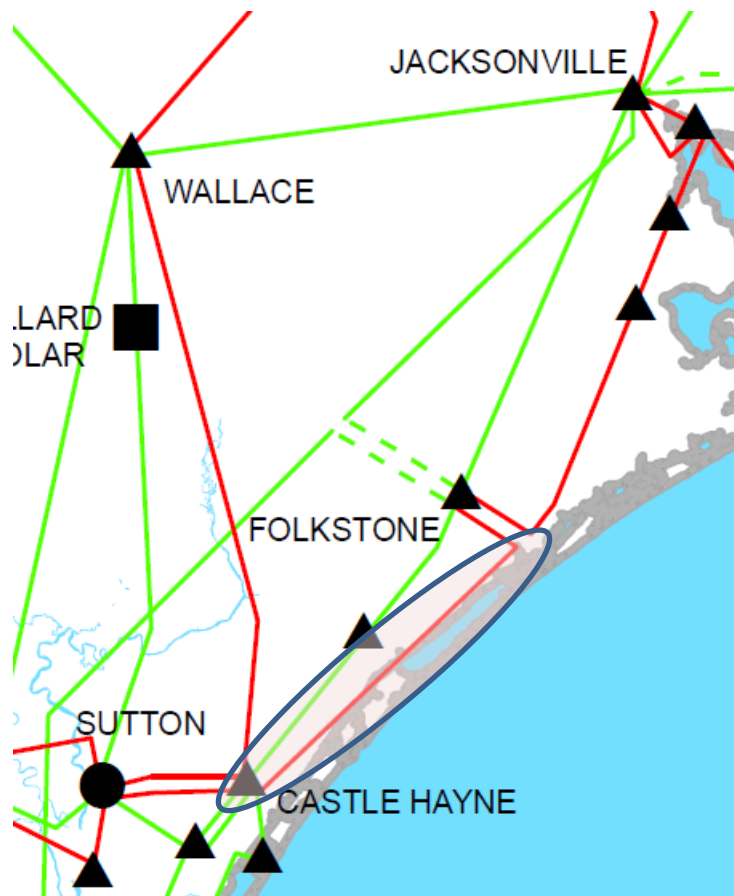
<b>Other Transmission Solutions Considered</b>
New 230 kV transmission lines.

<b>Why this Project was Selected as the Preferred Solution</b>
The cost and construction feasibility are much better with selected alternative.



## Castle Hayne–Folkstone 115 kV Line, Rebuild

- **NERC Category P1 violation**
- **Problem:** By winter 2028/29, an outage of the Castle Hayne–Folkstone 230 kV line will cause the Castle Hayne 230 kV Sub-Folkstone 115 kV line to overload. This project will mitigate the overload problem.
- **Solution:** Rebuild approximately 25.91 miles of 115 kV line (Castle Hayne 230 kV Sub to structure #251) with 1272 MCM ACSR or equivalent.





### Project ID and Name: 0057 – Holly Ridge North 115 kV Switching Station, Construct

<b>Project Description</b>
Construct a new 115 kV Switching Station northeast of Holly Ridge, NC where the Castle Hayne–Folkstone 115 kV and Folkstone–Jacksonville City 115 kV lines come together. Construct a new 115 kV feeder from the new switching station to Jones–Onslow EMC Folkstone POD.

<b>Status</b>	Conceptual
<b>Transmission Owner</b>	DEP
<b>Planned In-Service Date</b>	12/1/2028
<b>Estimated Time to Complete</b>	4 years
<b>Estimated Cost</b>	\$25 M

<b>Narrative Description of the Need for this Project</b>
By winter 2028-29, the NERC P2-1 opening of the Folkstone end of the Castle Hayne–Folkstone 115 kV line results in low voltages at stations on this line.

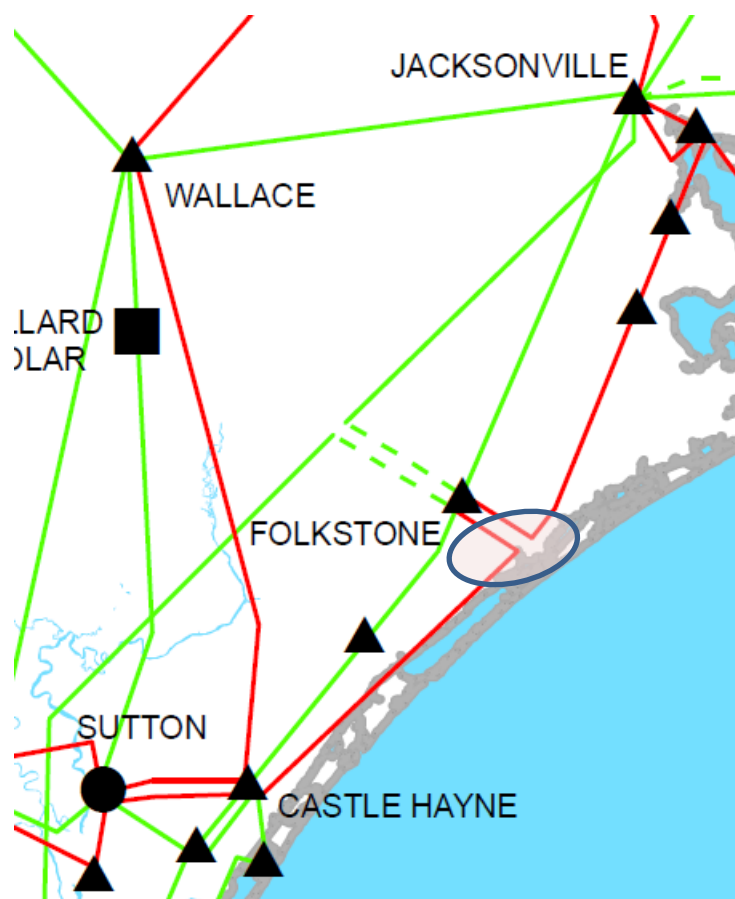
<b>Other Transmission Solutions Considered</b>
New 230 kV transmission lines.

<b>Why this Project was Selected as the Preferred Solution</b>
The cost and construction feasibility are much better with selected alternative.



## Holly Ridge North 115 kV Switching Station, Construct

- **NERC Category P2-1 violation**
- **Problem:** By winter 2028-29, the NERC P2-1 opening of the Folkstone end of the Castle Hayne – Folkstone 115 kV line results in low voltages at stations on this line.
- **Solution:** Construct new 115 kV switching station northeast of Holly Ridge.





# **Appendix D**

# **Collaborative Plan**

# **Comparisons**



# North Carolina Transmission Planning Collaborative

NCTPC Update on Major Projects – (Estimated Cost ≥ \$10M)								
Items identified in red are changes from the previous report.								
Project ID	Reliability Project	Transmission Owner	2019 Plan <sup>1</sup>			2020 Plan		
			Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>	Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>
0024	Durham–RTP 230 kV Line, Reconductor	DEP	Conceptual	TBD	15	Conceptual	TBD	20
0028	Brunswick #1–Jacksonville 230 kV Line Loop into Folkstone 230 kV Substation	DEP	Planned	6/1/2024	35	Removed	–	–
0031	Jacksonville–Grants Creek 230 kV Line and Grants Creek 230/115 kV Substation	DEP	Underway	6/1/2020	72	In-service	6/1/2020	72
0032	Newport–Harlowe 230 kV Line, Newport SS and Harlowe 230/115 kV Substation	DEP	Underway	6/1/2020	55	In-service	6/1/2020	55



# North Carolina Transmission Planning Collaborative

NCTPC Update on Major Projects – (Estimated Cost ≥ \$10M)								
Items identified in red are changes from the previous report.								
Project ID	Reliability Project	Transmission Owner	Status <sup>2</sup>	2019 Plan <sup>1</sup>		2020 Plan		
				Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>	Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>
0034	Sutton–Castle Hayne 115 kV North Line, Rebuild	DEP	Underway	12/31/2020	30	Underway	6/1/2021	30
0038	Harley 100 kV Lines (Tiger–Campobello), Reconductor	DEC	Conceptual	TBD	–	Removed	–	–
0039	Asheboro–Asheboro East 115 kV North Line, Reconductor	DEP	Underway	6/1/2020	24	Underway	6/1/2022	24
0042	Rural Hall 100 kV, Install SVC	DEC	Underway	4/1/2020	44	In-service	3/17/2020	44
0043	Orchard 230/100 kV Tie Station, Construct	DEC	Planned	12/1/2020	104	In-service	8/26/2020	104



# North Carolina Transmission Planning Collaborative

NCTPC Update on Major Projects – (Estimated Cost ≥ \$10M)								
Items identified in red are changes from the previous report.								
Project ID	Reliability Project	Transmission Owner	2019 Plan <sup>1</sup>			2020 Plan		
			Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>	Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>
0046	Windmere 100 kV Line (Dan River–Sadler), Construct	DEC	Planned	6/1/2023	23	Underway	8/1/2023	26
0048	Wilkes 230/100 kV Tie Station, Construct	DEC	Planned	12/1/2023	69	Underway	6/1/2024	69
0049	Ballantyne Switching Station, Construct	Underway	DEC	12/5/2019	23	In-service	12/5/2019	–
0050	Craggy–Enka 230 kV Line, Construct	DEP	Conceptual	12/1/2025	80	Conceptual	12/1/2026	80
0051	Cokesbury 100 kV Line (Coronaca–Hodges), Upgrade	DEC	Planned	6/1/2024	16	Planned	12/1/2024	16





# North Carolina Transmission Planning Collaborative

NCTPC Update on Major Projects – (Estimated Cost ≥ \$10M)								
Items identified in red are changes from the previous report.								
Project ID	Reliability Project	Transmission Owner	2019 Plan <sup>1</sup>			2020 Plan		
			Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>	Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>
0052	South Point Switching Station	DEC	–	–	–	Planned	12/1/2024	110
0053	Wateree 115 kV Plant, Upgrade 115/100 kV Transformers	DEP	–	–	–	Underway	12/1/2022	12
0054	Carthage 230/115 kV Substation, Construct Sub	DEP	–	–	–	Conceptual	12/1/2027	15
0055	Falls 230 kV Sub, Add 300 MVAR SVC	DEP	–	–	–	Conceptual	12/1/2028	50
0056	Castle Hayne–Folkstone 115 kV Line, Rebuild	DEP	–	–	–	Conceptual	12/1/2028	52



# North Carolina Transmission Planning Collaborative

NCTPC Update on Major Projects – (Estimated Cost ≥ \$10M)								
Items identified in red are changes from the previous report.								
Project ID	Reliability Project	Transmission Owner	2019 Plan <sup>1</sup>			2020 Plan		
			Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>	Status <sup>2</sup>	Projected In-Service Date	Estimated Cost (\$M) <sup>3</sup>
0057	Holly Ridge North 115 kV Switching Station, Construct	DEP	–	–	–	Conceptual	12/1/2028	25
<b>TOTAL</b>					<b>632</b>			<b>804</b>

<sup>1</sup> Information reported in Appendix B of the NCTPC 2019–2027 Collaborative Transmission Plan” dated January 17, 2020 and updated to reflect the mid-year plan report dated June 22, 2020 .

<sup>2</sup> Status: **In-service**: Projects with this status are in-service. This status was updated as of 12/1/2020.

**Underway**: Projects with this status range from the Transmission Owner having some money in its current year budget for the project to the Transmission Owner having completed some construction activities for the project.

**Planned**: Projects with this status do not have money in the Transmission Owner’s current year budget; and the project is subject to change.

**Conceptual**: Projects with this status are not *planned* at this time but will continue to be evaluated as a potential project in the future.

**Deferred**: Projects with this status were identified in the 2019 Report and have been deferred beyond the end of the planning horizon based on analysis performed to develop the 2020 Collaborative Transmission Plan.

**Removed**: Project is cancelled and no longer in the plan

<sup>3</sup> The estimated cost is in nominal dollars which reflects the sum of the estimated annual cash flows over the expected development period for the specific project (typically 2 – 5 years), including



## **North Carolina** Transmission Planning Collaborative

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direct costs, loadings and overheads; but not including AFUDC. Each year's cash flow is escalated to the year of the expenditures. The sum of the expected cash flows is the estimated cost.



# Appendix E

## Acronyms



## North Carolina Transmission Planning Collaborative

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### ACRONYMS

ACSR	Aluminum Conductor Steel Reinforced
ACSS/TW	Aluminum Conductor Steel Supported/Trapezoidal Wire
AEP	American Electric Power
AFUDC	Allowance for Funds Used During Construction
BAA	Balancing Authority Area
CC	Combined Cycle
CPLE	Carolina Power & Light East, or DEP East
CPLW	Carolina Power & Light West, or DEP West
CT	Combustion Turbine
DEC	Duke Energy Carolinas
DEP	Duke Energy Progress
DNR	Designated Network Resource
DVP	Dominion Virginia Power
ERAG	Eastern Interconnection Reliability Assessment Group
EU	Energy United
FSA	Facilities Study Agreement
GTP	North Carolina Global TransPark
ISA	Interconnection Service Agreement
kV	Kilovolt
LGIA	Large Generator Interconnection Agreement
LSE	Load Serving Entity
LTWG	SERC Long-Term Working Group
M	Million
MCM	Thousand Circular Mils
MMWG	Multiregional Modeling Working Group
MVA	Megavolt-Ampere
MVAR	Megavolt-Ampere Reactive
MW	Megawatt
NCEMC	North Carolina Electric Membership Corporation
NCEMPA	North Carolina Eastern Municipal Power Agency



## North Carolina Transmission Planning Collaborative

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NCMPA1	North Carolina Municipal Power Agency Number 1
NCTPC	North Carolina Transmission Planning Collaborative
NERC	North American Electric Reliability Corporation
NTE	NTE Energy
OASIS	Open Access Same-time Information System
OATT	Open Access Transmission Tariff
OSC	Oversight Steering Committee
OTDF	Outage Transfer Distribution Factor
PJM	PJM Interconnection, LLC
PMPA	Piedmont Municipal Power Agency
POD	Point of Delivery
PSS/E	Power System Simulator for Engineering
PWG	Planning Working Group
ROW	Right of Way
RTP	Research Triangle Park
SCEG	South Carolina Electric & Gas Company
SCPSA	South Carolina Public Service Authority
SE	Steam Electric (Plant)
SEPA	South Eastern Power Administration
SERC	SERC Reliability Corporation
SOCO	Southern Company
SS	Switching Station
SVC	Static VAR Compensator
TAG	Transmission Advisory Group
TRM	Transmission Reliability Margin
TSR	Transmission Service Request
TTC	Total Transfer Capability
TVA	Tennessee Valley Authority
VACAR	Virginia-Carolinas Reliability Agreement
VAR	Volt Ampere Reactive